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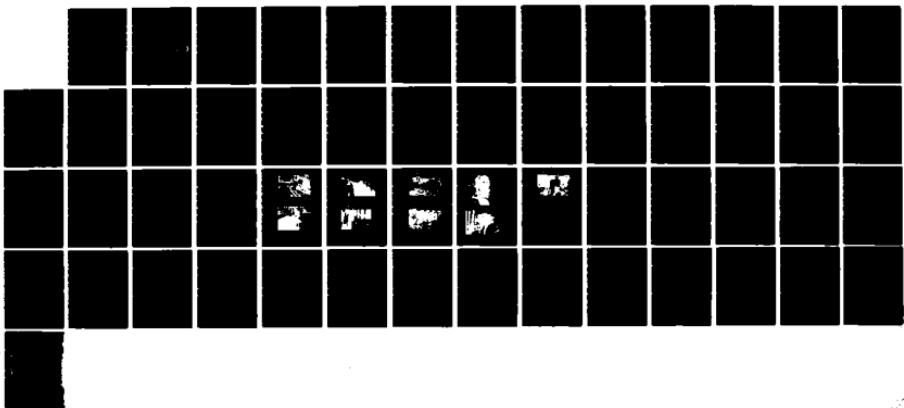
NATIONAL PROGRAM FOR INSPECTION OF NON-FEDERAL DAMS  
SUCCESS LAKE DAM CCT. (U) CORPS OF ENGINEERS WALTHAM MA  
NEW ENGLAND DIV MAY 81

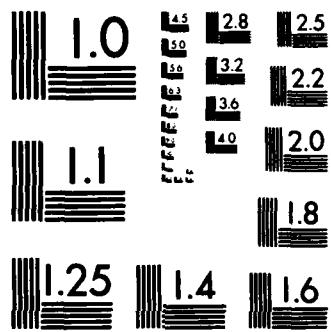
1/1

UNCLASSIFIED

F/G 13/13

NL





MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

AD-A142 830

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER CT 00079	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Success Lake Dam Conn. Coastal Basin, Bridgeport, Conn. NATIONAL PROGRAM FOR INSPECTION OF NON-FEDERAL DAMS		5. TYPE OF REPORT & PERIOD COVERED INSPECTION REPORT
7. AUTHOR(s) U.S. ARMY CORPS OF ENGINEERS NEW ENGLAND DIVISION		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS DEPT. OF THE ARMY, CORPS OF ENGINEERS NEW ENGLAND DIVISION, NEDED 424 TRAPELO ROAD, WALTHAM, MA. 02254		12. REPORT DATE May 1981
		13. NUMBER OF PAGES 50
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) APPROVAL FOR PUBLIC RELEASE: DISTRIBUTION UNLIMITED		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES Cover program reads: Phase I Inspection Report, National Dam Inspection Program; however, the official title of the program is: National Program for Inspection of Non-Federal Dams; use cover date for date of report.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) DAMS, INSPECTION, DAM SAFETY,  Success Lake Dam Conn. Coastal Basin Bridgeport, Conn.		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The Success Lake Dam, constructed in 1875, is a 132 ft. long, 17 ft. high structure composed of two earthfill embankments and a central 33 ft. long broad crested spillway. The original timber spillway decking has since been capped with concrete. There is a small single land bridge, across the overflow spillway section. Flow over the spillway is channeled through five 4 ft. wide, 2 ft. high openings, and one 3.3 ft. wide, 2 ft. high, opening formed by the bridge piers. The upstream concrete face of the spillway has a slope of approx. 2H:1V and the masonry downstream face is vertical.		

## SUCCESS LAKE DAM

CT 00079

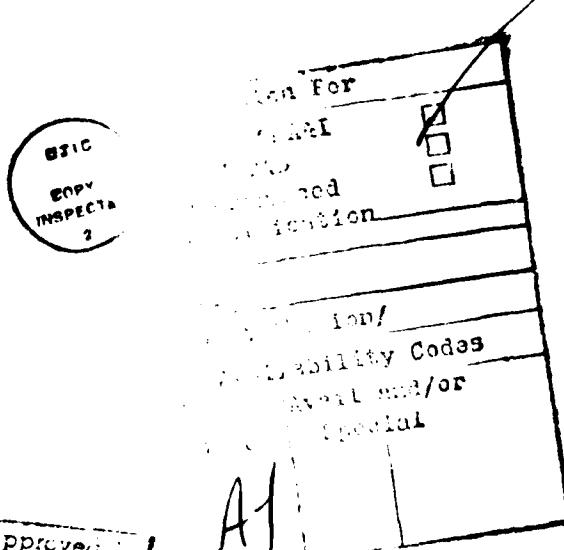
## **CONNECTICUT COASTAL BASIN**

## **BRIDGEPORT, CONNECTICUT**

## **PHASE I INSPECTION REPORT**

## NATIONAL DAM INSPECTION PROGRAM

MAY 1981



This document has been approved  
for public release and sale; its  
distribution is unlimited.

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CONSULTING  
ENGINEERS

**INTERNATIONAL ENGINEERING COMPANY, INC.**  
A MORRISON-KNUDSEN COMPANY

EASTERN DISTRICT OFFICE  
777 POST ROAD DARIEN CONNECTICUT 06820  
PHONE 203 656-3345

11410  
2616-110

May 7, 1981

Mr. E. P. Gould  
Project Management Branch  
Department of the Army  
New England Division  
Corps of Engineers  
424 Trapelo Road  
Waltham, Massachusetts 02154

Reference: Contract No. DACW33-81-C-0015  
Inspection and Evaluation of Non-Federal Dams  
FY-81, Southwestern Connecticut

Dear Mr. Gould:

The inspection of Success Lake Dam and subsequent hydrologic-hydraulic investigation revealed that the dam should be classified as having a low hazard potential. The following is an abbreviated Phase I Inspection report to substantiate this classification.

Sincerely,

*Reynold A. Hokenson*

Reynold A. Hokenson, P. E.  
Project Manager

RAH:mem

Enclosures

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JAN 1981 DAM INSPECTION PROGRAM

PAGE I INSPECTION REPORT

Identification No: CT 10079

Name of Dam: Success Lake Dam

Town: Bridgeport

County and State: Fairfield, Connecticut

Stream: Yellow Mill Channel

Dates of Inspection: February 5 and 19, 1981

BRIEF ASSESSMENT

The Success Lake Dam impounds Success Lake on the Yellow Mill Channel tributary in Bridgeport, Fairfield County, Connecticut. The structure is currently owned by Remington Arms Company, Inc., 939 Barnum Avenue, Bridgeport, Connecticut. The operation of the facility is the responsibility of Robert H. Gruss, Plant Engineer, Remington Arms Co., Inc., (203) 333-1112. Currently, the impoundment is maintained for aesthetics and wildlife conservation.

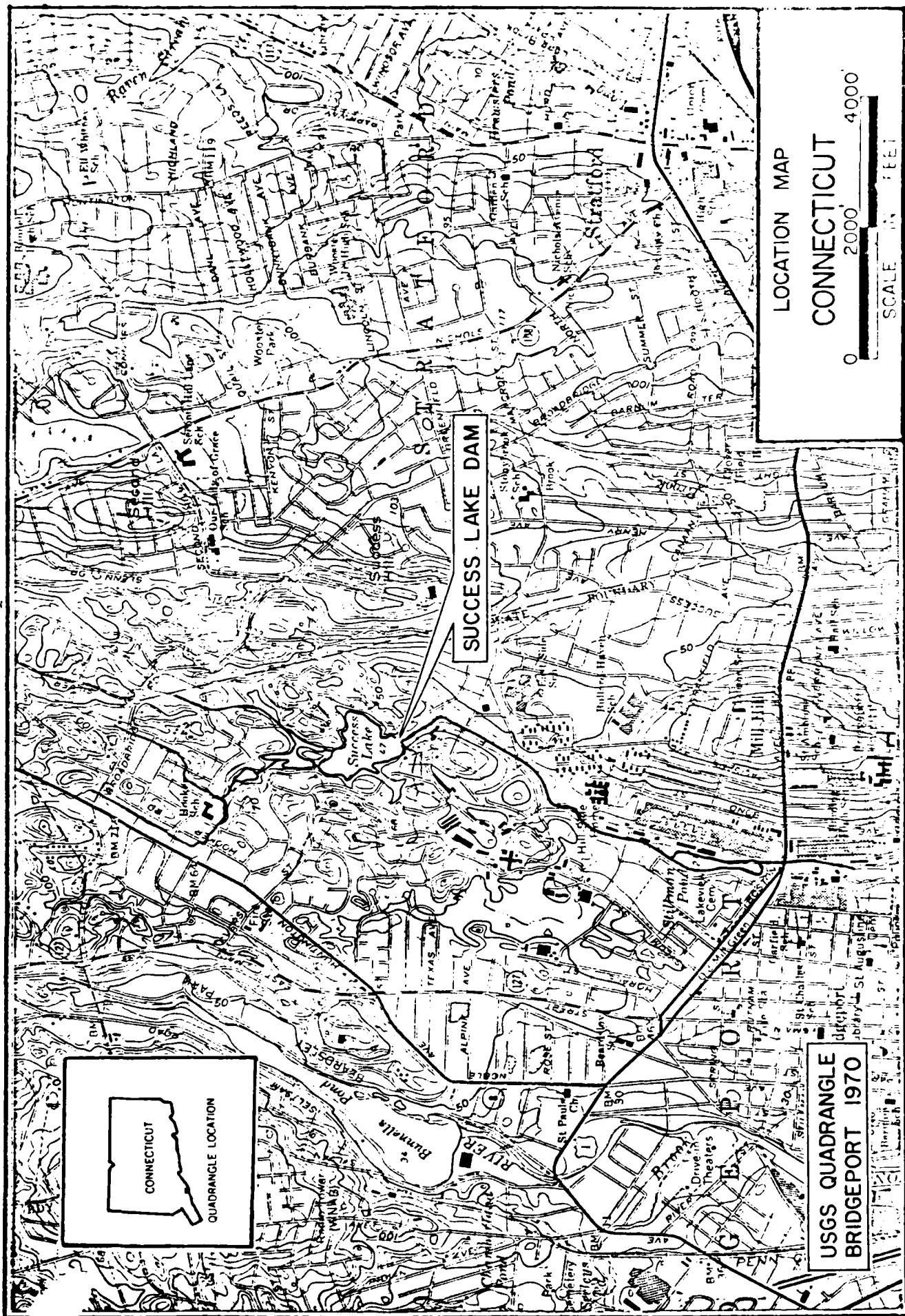
The Success Lake Dam, constructed in 1875, is a 132-foot-long, 17-foot-high structure composed of two earthfill embankments and a central 33-foot-long broad crested spillway. The original timber spillway decking has since been capped with concrete. There is a small single land bridge, across the overflow spillway section (Photo 1). Flow over the spillway is channeled through five 4-foot-wide, 2-foot-high openings, and one 3.3-foot-wide, 2-foot-high, opening formed by the bridge piers. The upstream concrete face of the spillway has a slope of approximately 2H:1V and the masonry downstream face is vertical. The downstream slopes of the two-side embankments are formed by vertical stone retaining walls. The upstream slopes also appeared to be vertical stone retaining walls, however, these areas were, for the most part, concealed beneath the water surface and accumulated sediments (Photos 2 and 3).

Two cast iron conduits pass through the earthfill embankment at the right abutment of the dam and provide additional outlets from the impoundment. A 14 inch diameter conduit exits the dam near its base approximately 12 feet from the right side of the spillway. Discharges from this conduit are regulated by a hand operated valve which is housed in a small masonry structure (Photo 9). The second conduit is 8 inches in diameter and emerges from the right embankment, approximately 5 feet below the top of the dam and about 25 feet from the spillway (Photo 7). This conduit extends 126 feet downstream to a small brick structure where, at one time, it provided water for the generation of steam (Photo 8). The brick structure formerly housed equipment for the generation and distribution of steam to the various industrial processes that were performed by Remington Arms Company, Inc., in the 1940's. This equipment was removed from the site and the building was converted to an employee locker room. The 8-inch conduit leading to this building, though deteriorated, is still intact.

Visual inspection of the site indicated that the dam is in poor condition. The inspection revealed the following: deterioration of the vertical downstream face of the spillway, cracked and missing portions of the concrete spillway crest along the downstream edge (Photo 4), cracks along the upstream and downstream interfaces of the spillway and abutments, exposed aggregate on the concrete spillway cap, seepage along the toe of the left embankment has resulted in a 20-foot by 30-foot marshy area approximately 40 feet from the dam, and a potentially inoperable low-level outlet. The seepage beneath the spillway, described in the inspection report submitted by William P. Sanders of the State of Connecticut Water Resource Commission on July 22, 1964 (see Correspondence), was not confirmed during the inspections conducted by IECO on February 2 and 19, 1981. During these inspections, an accumulation of rocks at the base of the spillway, ice formations on the downstream face of the spillway and particularly water flowing over the spillway made it impossible to examine this portion of the dam closely (Photos 5 and 6). Water was observed draining vertically through cracks in the concrete cap near the left upstream spillway abutment, but no corresponding of discharge was noted on the downstream

face of the spillway. In addition, localized outward movement of the stone retaining wall and the concrete spillway cap were also found in the vicinity of the left spillway abutment. The effected area is approximately 7 feet wide, but the movement has been slight and is a local condition not threatening the dam.

The Success Lake Dam has a maximum potential storage capacity of 119 acre-feet (ac-ft) and is approximately 17 feet in height. Since the dam falls within the Corp's criteria for the small size category based on storage (between 50 and 1,000 ac-ft), the dam is considered to be SMALL in size. The dam breach analysis was conducted in accordance with the "Rule of Thumb Guidance for Estimating Downstream Dam Failure Hydrographs", dated April 1978, and the potential impact area was defined. Failure of the dam would cause the water surface within the streambed immediately downstream of the dam to rise from 4.7 feet at a prefailure outflow of 310 cfs to 11.1 feet at an outflow of 2,360 cfs. The first floor of the brick structure located approximately 130 feet downstream from the dam is more than 20 feet above the streambed, and this will not be effected by the flood wave. The only remaining other structures adjacent to the Yellow Mill Channel are located 3,500 feet downstream from the dam. These will sustain little or no damage since the water surface within this reach will rise only 1.8 feet above the streambed. Since failure of the dam will cause little or no property damage and no loss of life, the dam has been classified as having a LOW hazard potential.



**APPENDIX A**

**INSPECTION CHECKLIST**

VISUAL INSPECTION CHECK LIST  
PARTY ORGANIZATION

PROJECT Success Lake Dam

DATE 02/5 & 19/81

TIME 10:00 a.m.

WEATHER Sunny, Cold

W.S. ELEV. 47.1

PARTY:

INITIALS:

1. Jeffrey T. Klaucke	JK
2. Myron B. Petrovsky	MP
3. Ernst H. Buggisch	EB
4. Paul Archer	PA
5. Harold Farnham	HF (Matthews Associates)

PROJECT FEATURE:

INSPECTED BY:

1. Dam	JK, MP, EB, PA
2. Intake Channel	JK, MP
3. Valvehouse	JK, HF, MP
4. Powerhouse Conduit	HF, JK, MP
5. Low Level Outlet	HF, JK, MP
6. Low level Outlet Channel	JK, MP, EB, PA
7. Spillway	JK, MP, EB
8. Bridge	JK, PA, EB

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam

DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Dam

NAME: JK, MP, EB, PA

AREA EVALUATED	CONDITION
<u>DAM EMBANKMENT</u>	
Crest Elevation	47.0
Current Pool Elevation	47.1
Maximum Impoundment to Date	Approximately 50.0
Surface Cracks	None
Pavement Condition	Good
Movement or Settlement of Crest	None
Lateral Movement	Local movement on upstream face near left spillway abutment.
Vertical Alignment	Good
Horizontal Alignment	Good
Condition at Abutment and at Concrete Structures	Cracks along U/S and D/S interfaces with spillway.
Indications of Movement of Structural Items on Slopes	Minor bulging of U/S and D/S retaining walls.
Trespassing on Slopes	None.
Sloughing or Erosion	None
Rock Slope Protection	The exposed U/S walls were irregular and missing stones.
Unusual Movement or Cracking at or near Toes	None
Unusual Embankment or Downstream Seepage	Wet area at D/S toe on the left bank. Seepage noted through valvehouse.
Piping or Boils	Possible piping along low level outlet conduit.

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Dam (Continued) NAME: JK, MF, EB, PA

AREA EVALUATED	CONDITION
Foundation Drainage Features	Unknown
Toe Drains	Unknown
Instrumentation System	None

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam

DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Intake Channel

NAME: JK, MP

AREA EVALUATED	CONDITION
<u>OUTLETS WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE</u>  a. Approach Channel  Slope Conditions  Bottom Conditions  Rock Slides or Falls  Log Boom  Debris  Condition of Concrete Lining  Drains or Weep Holes	Success Lake
b. Intake Structure  Condition of Concrete  Stop Logs and Slots	No structure visible above current pool level.

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam

DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Valvehouse

NAME: JK, HF, MP

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - CONTROL TOWER</u>	
a. Concrete and Structural	
General Condition	Fair, wooden roof rotted.
Condition of Joints	Good
Spalling	None
Visible Reinforcing	None
Rusting or Staining of Concrete	Near crack in valvehouse wall
Any Seepage or Efflorescence	Seepage noted through crack in valvehouse wall.
Joint Alignment	Good
Unusual Seepage or Leaks in Gate Chamber	None
Cracks	Right wall of valvehouse
Rusting or Corrosion of Steel	Exposed portion of low level outlet conduit.
b. Mechanical and Electrical	
Air Vents	
Float Wells	
Crane Hoist	
Elevator	
Hydraulic System	
Mechanical Valve	Not tested at owner's request
Emergency Gates	
Lightning Protection System	
Emergency Power System	
Wiring and Lighting System	

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam DATE: 02/5 & 19/81PROJECT FEATURE: Low level Outlet NAME: HF, JK, MP

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - TRANSITION AND CONDUIT</u>	
General Condition of Conduit	Fair
Rust or Staining on Conduit	Superficial rust on exposed conduit.
Spalling	N/A
Erosion or Cavitation	None
Cracking	None
Alignment of Monoliths	N/A
Alignment of Joints	N/A
Numbering of Monoliths	N/A
	<u>Note:</u> Only a small portion of the cast iron conduit (approximately 8 in.) was visible.

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam

DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Low Level Outlet Channel

NAME: JK, MP, EB, PA

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL</u>	
General Condition of Concrete	N/A
Rust or Staining	
Spalling	
Erosion or Cavitation	
Visible Reinforcing	
Any Seepage or Efflorescence	
Condition at Joints	
Drain holes	
Channel	
Loose Rock or Trees Overhanging Channel	Large rocks and 5 to 20 in. diameter trees were found immediately D/S of the outlet and adjacent to the spillway discharge channel.
Condition of Discharge Channel	Large rocks have accumulated on the channel floor.

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam

DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Spillway

NAME: JK, HF, EB

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS</u>	
a. Approach Channel	Success Lake
General Condition	
Loose Rock Overhanging Channel	
Trees Overhanging Channel	
Floor of Approach Channel	
b. Weir and Training Walls	
General Condition of Masonry	Loose stones in retaining walls, some stones missing and wall movements noted near spillway.
Rust or Staining	None
Spalling of spillway concrete cap	Near downstream edge of spillway weir.
Any Visible Reinforcing	None
Any Seepage	Some vertical drainage into dam through cracks in the spillway cap.
Drain Holes	None
c. Discharge Channel	
General Condition	Fair
Loose Rock Overhanging Channel	Loose rocks from downstream walls of spillway have accumulated in discharge channel.
Trees Overhanging Channel	Large tree on right bank between valvehouse and spillway.
Floor of Channel	Strewn with large rocks.
Other Obstructions	None

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake DamDATE: 02/5 & 19/81PROJECT FEATURE: BridgeNAME: JK, PA, EB

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - BRIDGE</u>	
a. Super Structure Bearings	N/A
Anchor Bolts	N/A
Bridge Seat	N/A
Longitudinal Members	N/A
Under Side of Deck	Good
Secondary Bracing	None
Deck	Good
Drainage System	All 3 inch diameter drains in curbs were free of obstructions.
Railings	Good
Expansion Joints	None
Paint	N/A
b. Piers	
General Condition of Concrete	Good
Alignment of Abutment	
Approach to Bridge	
Condition of Seat & Backwall	<u>Note:</u> The bridge is supported 2 feet above the spillway by 4 concrete piers that are founded on the spillway.

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Powerhouse Conduit NAME: JK, HF, MP

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - CONTROL TOWER</u>	
a. Concrete and Structural	
General Condition	N/A
Condition of Joints	
Spalling	
Visible Reinforcing	
Rusting or Staining of Concrete	
Any Seepage or Efflorescence	
Joint Alignment	
Unusual Seepage or Leaks in Gate Chamber	
Cracks	
Rusting or Corrosion of Steel	
b. Mechanical and Electrical	
Air Vents	
Float Wells	
Crane Hoist	
Elevator	
Hydraulic System	
Mechanical Valve	Valve inoperable, conduit has not been used since the 1940's.
Emergency Gates	
Lightning Protection System	
Emergency Power System	
Wiring and Lighting System	

APPENDIX B

ENGINEERING DATA

SUMMARY OF DATA AND CORRESPONDENCE

<u>DATE</u>	<u>TO</u>	<u>FROM</u>	<u>SUBJECT</u>	<u>PAGE</u>
			Water Resources Inventory Data	B-2
6/7/66	Mr. W.H. O'Brien III Water Resources Commission State of Connecticut	Joseph W. Cone Civil Engineer	Inspection	B-3
10/9/64	State of Connecticut Water Resources Commission State of Connecticut	J. P. Barry Works Engineer Remington Arms Company, Inc.	Verification upon completion of suggested repairs	B-6
7/22/64	H.M. Pierce Jr. Plant Manager Remington Arms Company, Inc.	William P. Sander Engineer-Geologist State of Connecticut	Suggested spillway repairs	B-7
			COE Inventory Data	B-8

No. \_\_\_\_\_

WATER RESOURCES UNIT  
SUPERVISION OF DAMS  
INVENTORY DATA

Inventoried  
By \_\_\_\_\_

Lat:  $41^{\circ}$  12.3'

Date \_\_\_\_\_

Long:  $73^{\circ}$  9.9'

Name of Dam or Pond SUCCESS LAKE

Code No. \_\_\_\_\_

Nearest Street Location Huntington Turnpike

Town Bridgeport

U.S.G.S. Quad. Bridgeport

Name of Stream Unnamed

Owner Remington Arms Company, Inc.

Address Barnum Avenue

Bridgeport, CT

Pond Used For Fire Protection Drainage Area 2.43 sq. mi.

Dimensions of Pond: Width 700' Length 1100' Area 18.3 ac.

Total Length of Dam 125' Length of Spillway 35'

Location of Spillway Center of dam

Height of Pond Above Stream Bed 15'

Height of Embankment Above Spillway 3'

Type of Spillway Construction Concrete cap

Type of Dike Construction Masonry

Downstream Conditions Bridgeport

Summary of File Data \_\_\_\_\_

Remarks \_\_\_\_\_

Would Failure Cause Damage? \_\_\_\_\_ Class \_\_\_\_\_

NEW YORK LICENSE 4755  
CONNECTICUT REGISTRATION 4

JOSEPH W. CONE  
CIVIL ENGINEER  
124 HAVEMEYER PLACE  
GREENWICH, CONNECTICUT  
06830

STATE TOWNSEND 9-2152 TELEPHONE  
COMMISSION RECEIVED

June 7, 1966

JUN 10 1966

ANSWERED  
REFERRED  
FILED

Mr. William H. O'Brien III  
Water Resources Commission  
State Office Building  
Hartford 15, Conn.

Re: Dam #46 Stillman Pond-Bdpt.  
A.V.D SUCCESS LAKE D.A.Y

Dear Mr. O'Brien:

As requested, I have inspected the Stillman Pond Dam and the tributary watershed. Also permission was obtained from Remington Arms office to inspect Success Lake Dam, being escorted by one of their guards, since the condition of this dam is involved with Stillman.

	Success	Stillman
Watershed	2.28 sq.mi.	3.44 sq. mi.
Peak Q pres 100 yr	1250 cfs	1890 cfs
" " 2000 AD 400 yr	4370 "	5130 "

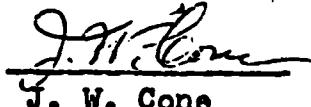
Both dams are solidly constructed and, in my opinion, will not fail but both will be overtopped in the future. Both have very low headroom, Success 6 openings averaging 4'x2'; openings were not measured at Stillman, it was evident that dam is safe although it will be overtopped.

Tracks serving the G.E. Plant will be flooded in the future during a severe storm due to channel of inadequate capacity.

Copies of work sheets, three photos and map of watersheds are enclosed. See Lake Forest for more applicable data.

My recommendation is that your office suggest to Remington Arms and General Electric that there be a standing order that their maintenance men see to it that openings at dams be kept clear of debris during heavy storms, this to reduce frequency of overtopping.

Very truly yours,

  
J. W. Cone

JWC/dr  
Enc: 6

Topographic Sheet

FOREST  $\frac{125 \text{ Ac}}{25 \text{ yr. forest}} = 1.45 \text{ sp.mi}$   $RF = 1.2$

(cont'd)  $Q_{\text{peak}} = 850 \text{ cfs}$  Wanted P.D.

Forest should develop rapidly. Rolling terrain.

$Q_{\text{present}} 25 \text{ yr} = RF \times LF \times FF \times Q$

$$= 1 \times 0.8 \times 1 \times 250 = 680 \text{ cfs} \quad 0.73$$

$$Q_{\text{ " }} 100 \text{ yr} = 1 \times 0.8 \times 1.8 \times 250 = 1220 \quad 1.22$$

$$Q_{\text{ " }} 400 \text{ yr} = 1 \times 0.8 \times 3.8 \times 250 = 2580 \quad 2.8$$

$$\text{" 2000AD" } = 1 \times 1.0 \times 3.8 \times 250 = 3240 \quad 3.5$$

Compare 3240 with 1955 Floods. 1.5 sp.mi.  $Q = 5000 \text{ cfs} = 4150 \text{ ft}^3/\text{s}$   
 $= 6000 \text{ m}^3/\text{s}$  1945

SUCCESS  $\frac{1460 \text{ Ac}}{25 \text{ yr}} = 2.28 \text{ sp.mi}$

Entire area developing rapidly except 132 Ac occupied by P.C. Forest  
 Rolling terrain rather flat

Chart A  $Q = 1150 \text{ cfs}$

$Q_{\text{peak}} 25 \text{ yr} = RF \times LF \times FF \times Q$

constant  
685

$$= 1 \times 0.5 \times 1 \times 1150 = 680 \text{ cfs} \quad 0.97$$

$$\text{" 100 } = 1 \times 0.5 \times 1.8 \times 1150 \quad 1250 \quad 0.85$$

$$\text{" 400 } = 1 \times 0.5 \times 3.8 \times 1150 \quad 2220 \quad 1.3$$

$$\text{" 2000AD" } = 1 \times 1.0 \times 3.8 \times 1150 \quad 4370 \quad 3.0$$

Provided River flows controls. Large area.

STILLING  $\frac{2200 \text{ Ac}}{34457 \text{ mi}} \text{ Chart A } Q = 1500$

constant  
455

$Q_{\text{peak}} 25 \text{ yr} = RF \times LF \times FF \times Q$

$$= 1 \times 0.7 \times 1 \times 1500 = 1050 \quad 0.48 \text{ cfs/ft.}$$

$$\text{" 100 } = 1 \times 0.7 \times 1.8 \times 1500 \quad 1890 \quad 0.85$$

$$\text{" 400 } = 1 \times 0.7 \times 3.8 \times 1500 \quad 4000 \quad 1.8$$

$$\text{" 2000AD" } = 1 \times 0.9 \times 3.8 \times 1500 \quad 5130 \quad 2.3$$

Provided from Areas of G.F. do not exceed 330 Ac.

J.V.L.  
5/13/19

# Forest & Stream

5/4/66  
5/16

## Lake Forest #25

580	watershed
2155	Circa 578 sq mi
<u>5775</u>	<u>1.043 sq mi</u>
	<u>925 Ac</u>

Lake Area
3.42
2.52
41.42
.105 sq mi

Long Dist 5.55
1.02
105 sq mi

Storage Ratio 1:14

Fair

Area Success	acre	Storage
Watershed		Lake Area
913		0.18
118.24		0.46
<u>4</u> <u>9.12</u>		<u>4</u> <u>1.53</u>
2.28 sq mi		.038 sq mi
140 Ac		24 Ac

Total Area
40.16 sq mi
11.82
.205 sq mi
132 Ac

Storage Ratio 1:61 Very Poor

## Stillman Park below Success

Total Watershed	Lake Area
4.70	0.03
1.25	.01
1.12 sq mi	.003 sq mi
72.0 Ac	9.0 Ac

Owned by Bear River  
to G.E. trib to  
Stillman including  
trib to Success

42.0	.515	320 Ac.
------	------	---------

Storage Ratio 1:83 Very Bad practically 0

## TOTAL Stillman #46 (includes Success)

Watershed	Lake Surface	Lengthed 3.15 mi
13.76	Acreage 1.12 "	Width 1.12 "
27.55		
<u>4</u> <u>13.77</u>		
3.44 sq mi		
2200 Ac	Success 24 Ac	
1460	Stillman 9	
780	Total 33 Ac	

2210 Chis.
------------

Total Storage Ratio 1:67 Very poor

*Remington*

*PETERS*

# REMINGTON ARMS COMPANY, INC.

MANUFACTURERS OF  
SPORTING FIREARMS, AMMUNITION

TRAPS

TARGETS

POWER TOOLS

ARMS AND CARTRIDGE POWERED TOOLS  
ILION, N. Y.

AMMUNITION, BRIDGEPORT, CONN.  
POWER TOOLS, PARK FOREST, ILL.

BRIDGEPORT 2, CONNECTICUT

PETERS CARTRIDGE DIVISION  
BRIDGEPORT, CONN  
TRAPS AND TARGETS, FINDLAY, OHIO  
CABLE - HARTLEY, BRIDGEPORT  
- ALL CODES -

October 9, 1964

SUCCESS LAKE DAM  
BRIDGEPORT

State of Connecticut  
Water Resources Commission  
State Office Building  
Hartford 15, Connecticut

Attention Mr. William P. Sander, Engineer-Geologist

Gentlemen:

Reference - Your letter of July 22, 1964

The leakage under the spillway is a condition we are aware of and have been checking periodically. There is no apparent increase in the water flow over the past ten years and we, therefore, feel this is not a condition to cause concern. The massive construction of this dam should be adequate if the leaks do not become larger, or general deterioration set in.

We have a periodic inspection set up whereby the quantity of water leaking is measured and checked against previous findings. Any increase will be readily recognized and prompt remedial action will be taken.

The trees specified in your report have been removed.

Very truly yours,

REMININGTON ARMS COMPANY, INC.  
H.M. PIERCE, JR., WORKS MANAGER

*J.P. Barry*  
J. P. Barry  
Works Engineer

JPB:O'L

STATE WATER RESOURCES COMMISSION RECEIVED	
OCT 13 1964	
ANSWERED _____	B-6
REFERRED _____	
FILED _____	

July 22, 1964

Mr. H. M. Pierce, Jr., Plant Manager  
Remington Arms Company, Inc.  
Barnum Avenue  
Bridgeport, Connecticut

Dear Sir:

The Water Resources Commission has recently completed an inventory of all the dams in the Town of Bridgeport.

During the inventory, the dam forming Success Lake was inspected and was found to be in need of repair. At the date of the inspection, all stream flow was through leakage under the spillway. In addition, the trees which are growing on the dam should be removed. These points are not critical at the present time but represent a condition which could lead to failure of the dam.

We would appreciate hearing what plans you have to place this structure in a safe condition.

Very truly yours,

William P. Sander  
Engineer - Geologist

WPS:js

Call to reserve clearance. On days notice.

Bob Gross Sat 13/6

AEROTRAINS CONTROL SYMBOL  
OAGEN - CNGF - 11

better approx. time & date  
blocks

**APPENDIX C**

**PHOTOGRAPHS**

— SUCCESS LAKE —

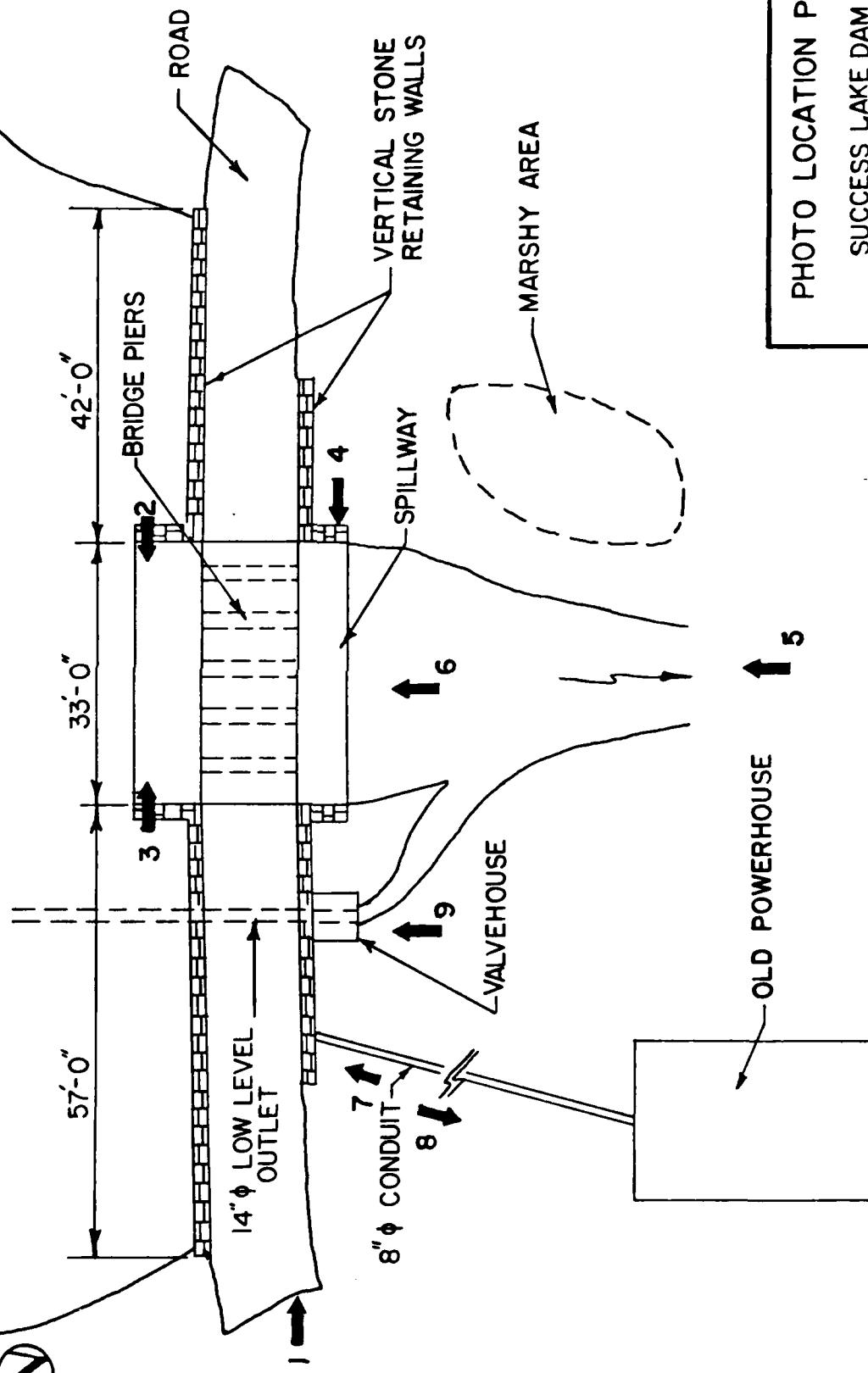




Photo 1 Top of dam and single lane road.



Photo 2 Upstream face of dam, spillway crest and right dam embankment.



Photo 3 Upstream face of dam, spillway crest and left dam embankment.



Photo 4 Downstream spillway crest and bridge piers.



Photo 5 Downstream face of dam.



Photo 6 Downstream masonry face of spillway.



Photo 7 Downstream masonry face  
of right dam embankment,  
8 inch diameter conduit  
and control valve.



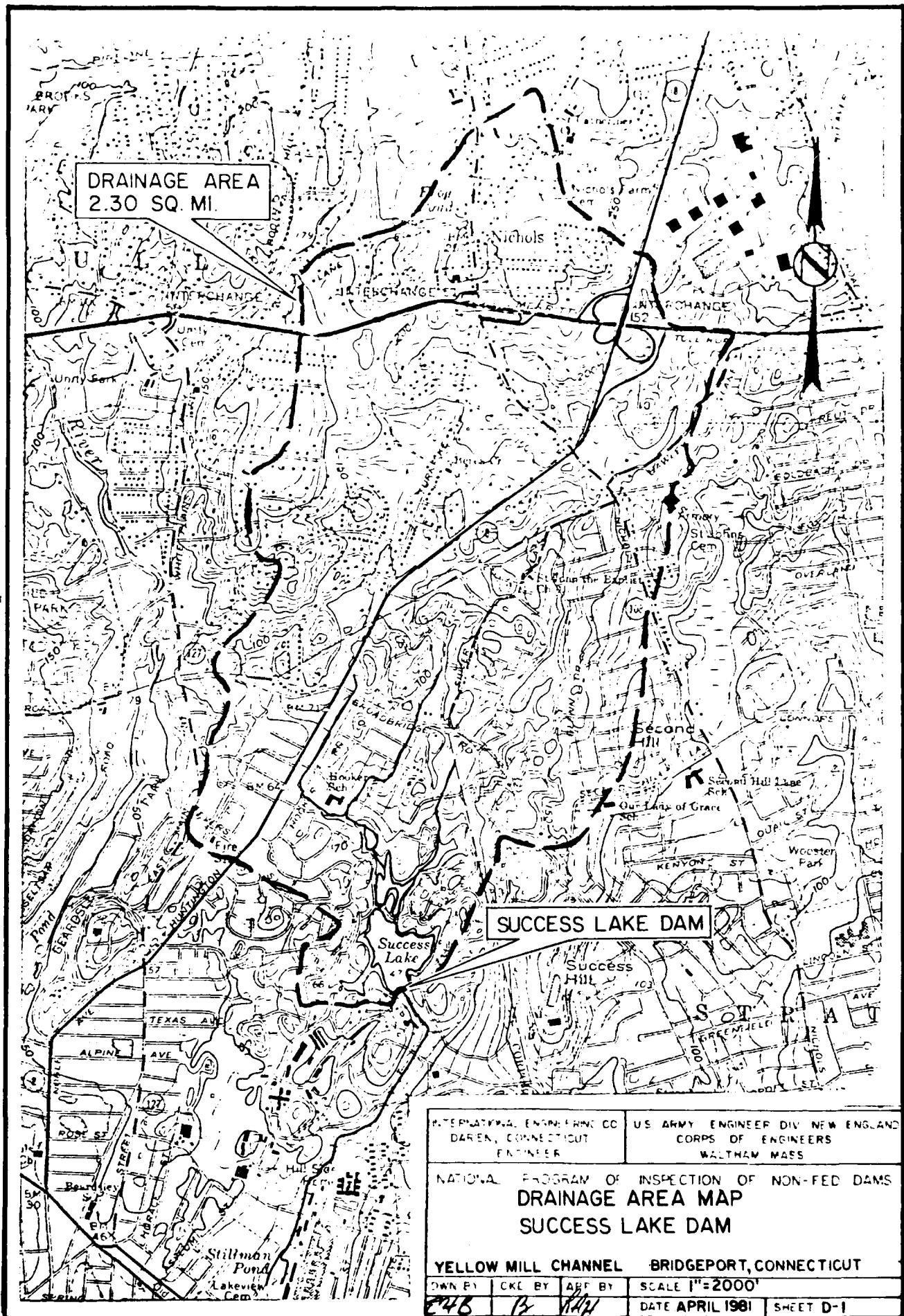
Photo 8 Brick structure and 8 inch diameter conduit.



Photo 9 Low-level outlet and valvehouse.

**APPENDIX D**

**HYDROLOGIC AND HYDRAULIC COMPUTATIONS**





INTERNATIONAL ENGINEERING COMPANY, INC.

Project NATIONAL DAM INSPECTION PROGRAM (NDIP)  
Feature SUCCESS LAKE DAM, BRIDGEPORT, CT  
Item CT00079

Sheet D-1  
Contract No. 2616-04  
File No.   
Designed M.P.  
Date 3/10/81  
Checked A.J.F.  
Date

## HYDRAULIC / HYDROLOGIC INSPECTION

SUCCESS LAKE DAM, BRIDGEPORT, CT CT00079

### I. PERFORMANCE AT PEAK FLOOD CONDITIONS

1. MAXIMUM PROBABLE FLOOD

2. WATERSHED CLASSIFIED AS "ROLLING"

3. WATERSHED AREA (D.A.) = 2.30 SQ. MI. \*

\* FROM IECO MEASUREMENTS ON THE BRIDGEPORT USGS QUADRANGLE MAP, CT. FROM U.S. CORPS OF ENGINEERS (ACE) DATA, D.A. IS 2.13 SQ. MI.

4. EXTRAPOLATING FROM NED-ACE GUIDE CURVES

PMF ≈ 2080 CFS / SQ. MI.

d. THEREFORE, PEAK INFLOW:

$$\text{PMF} = 2080 \times 2.3 \approx 4780 \text{ CFS}$$

$$\frac{1}{2} \text{ PMF} \approx 2390 \text{ CFS}$$

2. SURCHARGE AT PEAK INFLOWS (PMF AND  $\frac{1}{2}$  PMF).

a. OUTFLOW RATING CURVE

i. SPILLWAY

THE MASONRY SPILLWAY IN THE MID-SECTION OF SUCCESS LAKE DAM IS

A BROAD-CRESTED WEIR WITH A VERTICAL DOWNSTREAM FACE

(SEE SKETCHES ON P.D-2).



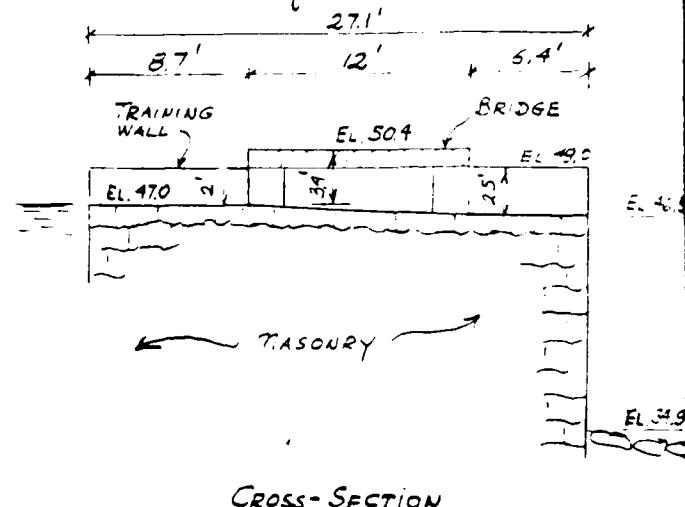
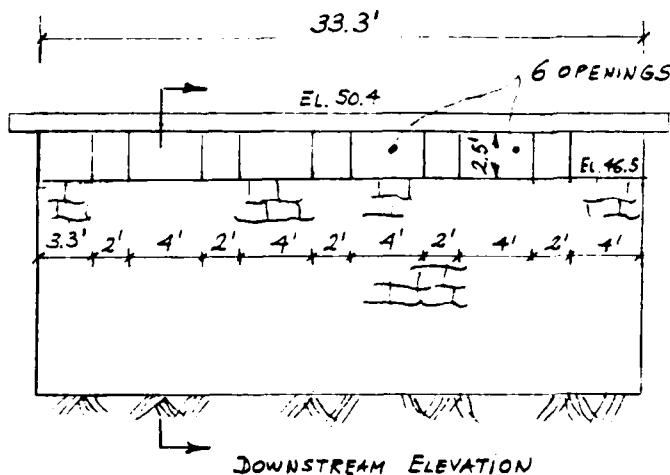
D-1



INTERNATIONAL ENGINEERING COMPANY, INC.

Project NO. 10  
 Feature SUCCESS LAKE DAM  
 Item \_\_\_\_\_

Contract No. 266-C Sheet D-2  
 File No. \_\_\_\_\_  
 Designed M.P. Date 3-5-61  
 Checked J.F. Date \_\_\_\_\_



THE 33.3-FT-WIDE AND 27.1-FT-LONG SPILLWAY HAS A CONCRETE ROAD BRIDGE

WITH 6 OPENINGS THE FIVE OF WHICH HAVE A WIDTH OF 4 FT AND THE ONE  
 OPENING ON THE RIGHT SIDE IS A 3.3-FT WIDE. THE HEIGHT OF THE OPENINGS IS  
 2 FT ON THE UPSTREAM BRIDGE EDGE AND 2.5 FT ON THE DOWNSTREAM EDGE.

THE TOTAL LENGTH OF THE OPENINGS IS  $L_o$  FT AND THE TOTAL AREA OF

THE OPENINGS ON THE UPSTREAM SIDE IS  $A_o$  SQ. FT.

ASSUMING  $C_1 = 2.2$  ( $H < 2$  FT) AND  $C_2 = 0.6$  ( $H > 2$  FT) AND ADOPTING  
 THE SPILLWAY CREST ELEV. 47.0 AS DATUM, THE SPILLWAY DISCHARGE IS  
 APPROXIMATING BY :

$$Q_s = C_1 L_o H_1^{3/2} + C_2 A_o \sqrt{2g(H_2 - \frac{3}{2})^{\frac{1}{2}}} = 2.2 \times 23.3 \times H_1^{3/2} + 0.6 \times 16.6 \times \sqrt{64.4(H_2 - \frac{3}{2})^{\frac{1}{2}}}$$

$$Q_s = 51.3 H_1^{3/2} + 224.4(H_2 - \frac{3}{2})^{\frac{1}{2}} \quad (\text{WHEN } H_1 < 2 \text{ FT}, H_2 = \frac{3}{2}; \text{ WHEN } H_2 > 2, H_1 = 0)$$





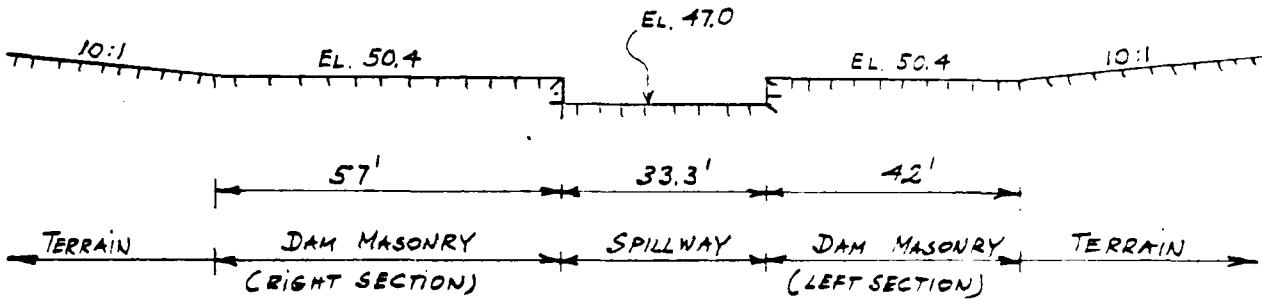
INTERNATIONAL ENGINEERING COMPANY, INC.

Project NDIP  
 Feature SUCCESS LAKE DAM  
 Item \_\_\_\_\_

Contract No. 566-54 Sheet 2-3  
 File No. \_\_\_\_\_  
 Designed MP Date 3-0-5  
 Checked Df Date 15

ii. EXTENTION OF THE RATING CURVE FOR SURCHARGE OVERTOPPING THE DAM  
 AND/OR ADJACENT TERRAIN

THE SUCCESS LAKE DAM IS A MASONRY STRUCTURE WITH A TOP ELEVATION  
 OF 50.4 AND TOTAL LENGTH OF 99 FT. THE TERRAINS ADJACENT TO  
 THE DAM HAVE SLOPES APPROXIMATELY 10:1 (SEE SKETCH BELOW).



DUE TO THE IRREGULARITIES IN THE PROFILE AN EQUIVALENT WEIR LENGTH  
 MUST BE COMPUTED. ASSUMING A DISCHARGE COEFFICIENT  $C=2.3$   
 AND ADOPTING THE SPILLWAY CREST AS DATUM (EL. 47.0), THE OVERFLOW  
 CAN BE APPROXIMATED BY THE FOLLOWING EQUATIONS:

(1) TOP OF DAM AT EL. 50.4.

$$Q_d = 2.3 \times \frac{137.3}{128.3} \times (H_3 - 3.4)^{3/2} = 304.3 (H_3 - 3.4)^{3/2}, \quad (H_3 > 3.4 \text{ ft})$$

(2) SLOPING TERRAIN TO THE LEFT AND RIGHT OF THE DAM:

$$L_s = \left(\frac{2}{5}\right) \times (H_3 - 3.4) = \left(\frac{2}{5}\right) 10 (H_3 - 3.4) = 4(H_3 - 3.4)$$

$\therefore$  DISCHARGE OVER LEFT AND RIGHT TERRAINS

$$Q_s = 2L_s (H_3 - 3.4)^{3/2} = 2 \times 4 (H_3 - 3.4)^{3/2} = 8 (H_3 - 3.4)^{5/2}$$





INTERNATIONAL ENGINEERING COMPANY, INC.

Project NDIP

Feature SUCCESS LAKE DAM

Item

Contract No. 2616-C4

Sheet D-4

Designed M.P.

File No.

Checked R.F.

Date 3/10/81

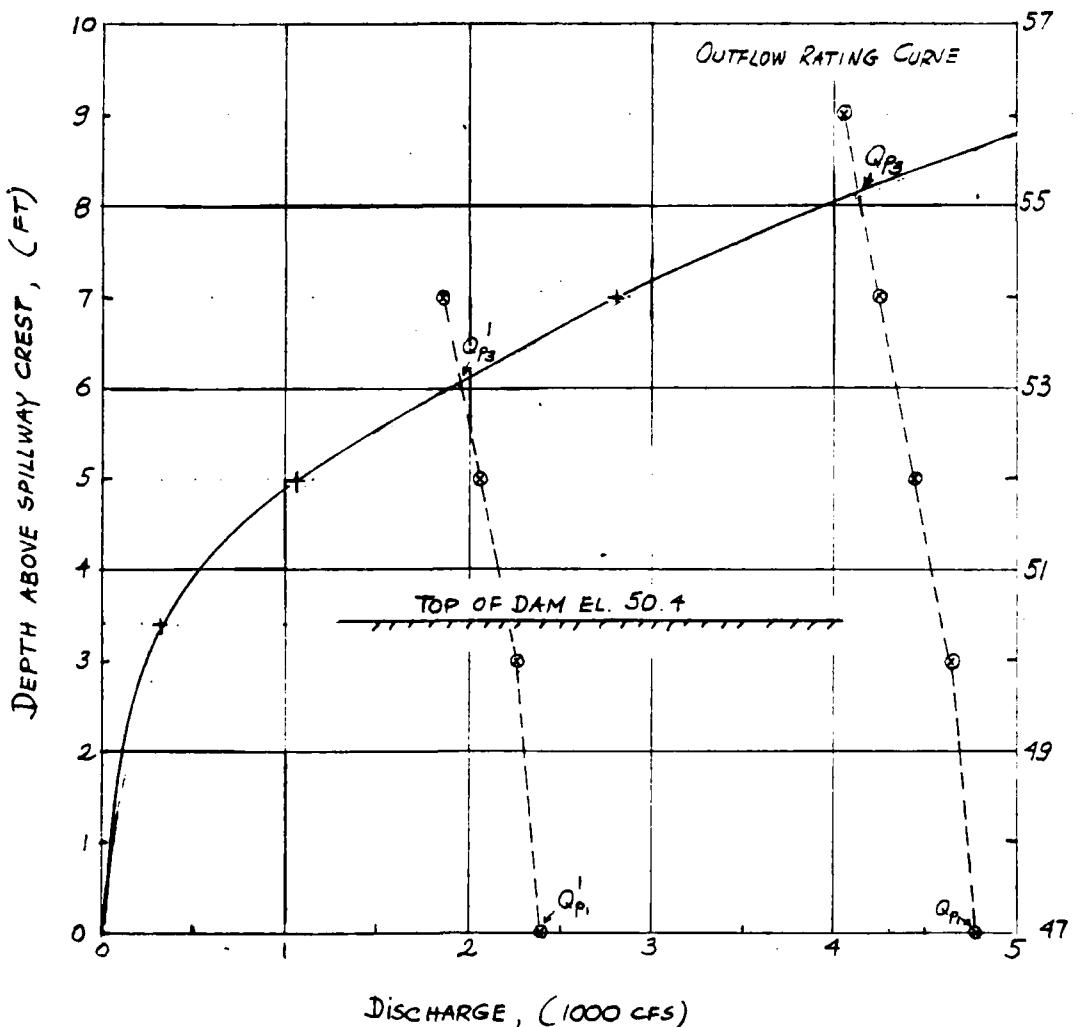
Date

THEREFORE, THE TOTAL OUTFLOW RATING CURVE IS APPROXIMATED BY:

$$Q = 51.3 H_1^{3/2} + 224.4 \left(H_2 - \frac{3}{2}\right)^{3/2} + 304.3 (H_3 - 3.4)^{3/2} + 8(H_3 - 3.4)^{5/2} \quad H_3 \geq 3.4$$

WHEN  $H_1 < 2$  FT,  $H_2 = \frac{3}{2}$ ; WHEN  $H_2 > 2$ ,  $H_1 = 0$ 

THE RESULTING OUTFLOW RATING CURVE IS AS FOLLOWS:



WATER SURFACE ELEVATIONS, (FT- NGVD)



D-4



INTERNATIONAL ENGINEERING COMPANY, INC.

Project

NDIP

Feature

SUCCESS LAKE DAM

Item

Contract No. 2616-CF

Sheet D-5

File No.

Designed MP

Date 3/10/68

Checked P.F.

Date

b. SURCHARGE HEIGHT TO PASS PEAK INFLOWS ( $Q_p$  AND  $Q_p'$ )

i. @  $Q_p = 4780 \text{ CFS}$   $H_s \approx 8.6 \text{ FT}$

ii. @  $Q_p' = 2390 \text{ CFS}$   $H_s' \approx 6.6 \text{ FT}$

## c. EFFECT OF SURCHARGE STORAGE ON PEAK OUTFLOWS :

## i. AVERAGE POND AREA WITHIN EXPECTED SURCHARGE:

(1) POND AREA AT FLOW LINE (EL. 47.0)  $A_{47}^* = 12.85 \text{ AC}$

(2) POND AREA AT EL. 50.0  $A_{50}^* = 30.3 \text{ AC}$

(3) AREA AT CONTOUR 60.0  $A_{60}^* = 68.8 \text{ AC}$

\* FROM IECO MEASUREMENTS ON THE BRIDGEPORT USGS QUADRANGLE MAP, CT

ASSUMING NORMAL POOL AT SPILLWAY CREST EL. 47.0, APPROXIMATING

STAGE-STORAGE RATING CURVE WAS CONSTRUCTED (SEE A D-6).

ii. DISCHARGE ( $Q_{p_s}$ ) AT VARIOUS HYPOTHETICAL SURCHARGE ELEVATIONS :

$H = 9 \text{ FT}, \quad V = 362 \text{ AC-FT}, \quad \therefore S = \frac{362}{2.3 \times 53.3} = 2.95 \text{ IN}$

$H = 7 \text{ FT}; \quad V = 262 \text{ AC-FT}; \quad S = 2.14 \text{ IN}$

$H = 5 \text{ FT}; \quad V = 162 \text{ AC-FT}; \quad S = 1.32 \text{ IN}$

$H = 3 \text{ FT}; \quad V = 65 \text{ AC-FT}; \quad S = 0.53 \text{ IN}$



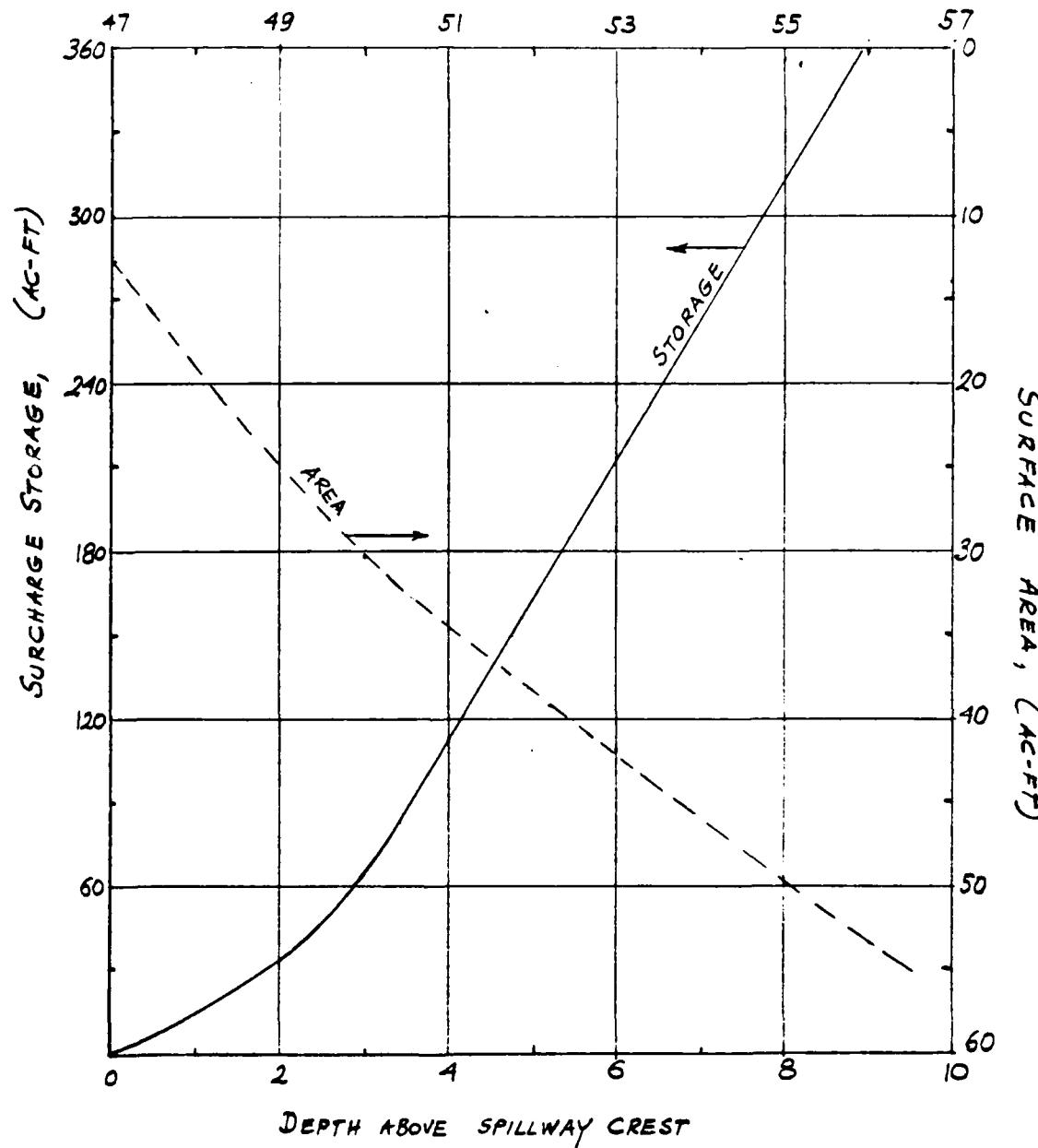


INTERNATIONAL ENGINEERING COMPANY, INC.

Project NDI<sup>o</sup>  
Feature SUCCESS LAKE DAM  
Item \_\_\_\_\_Contract No. E66-04  
Designed M.P.  
Checked RJF  
File No. \_\_\_\_\_  
Date 3/0/81  
Date \_\_\_\_\_

## STAGE-STORAGE AND STAGE-AREA CURVES

SURFACE ELEVATIONS, (FT- NGVD)





INTERNATIONAL ENGINEERING COMPANY, INC.

Project NDIP Contract No. 2E-E-04 Sheet D-7  
 Feature SUCCESS LAKE DAM File No. \_\_\_\_\_  
 Item \_\_\_\_\_ Designed NDP Date 5/28/  
 Checked by JF Date \_\_\_\_\_

FROM APPROXIMATE ROUTING NED-ACE GUIDELINES AND 19 IN MAXIMUM PROBABILITY

RUNOFF IN NEW ENGLAND:

$$Q_{P_2} = Q_{P_1} \left(1 - \frac{s}{19}\right) \text{ AND FOR } \frac{1}{2} \text{ PMF } Q_{P_2}' = Q_{P_1}' \left(1 - \frac{s}{3.5}\right)$$

∴ FOR THE PREVIOUS HYPOTHETICAL SURCHARGES:

$$H = 9 \text{ FT}, \quad Q_{P_2} = 4038 \text{ CFS}, \quad Q_{P_2}' = 1648 \text{ CFS}$$

$$H = 7 \text{ FT}, \quad Q_{P_2} = 4242 \text{ CFS}, \quad Q_{P_2}' = 1852 \text{ CFS}$$

$$H = 5 \text{ FT}, \quad Q_{P_2} = 4448 \text{ CFS}, \quad Q_{P_2}' = 2058 \text{ CFS}$$

$$H = 3 \text{ FT}, \quad Q_{P_2} = 4647 \text{ CFS}, \quad Q_{P_2}' = 2257 \text{ CFS}$$

d. PEAK OUTFLOWS ( $Q_{P_3}$  AND  $Q_{P_3}'$ ):

USING NED-ACE GUIDELINES "SURCHARGE STORAGE ROUTING" ALTERNATE

METHOD AND RATING CURVE (SEE P. D-4):

$$Q_{P_3} = 4120 \text{ CFS} \quad H_3 = 8.1 \text{ FT}$$

$$Q_{P_3}' = 1950 \text{ CFS} \quad H_3' = 6.05 \text{ FT}$$

3. SPILLWAY CAPACITY RATIO TO PEAK INFLOW AND OUTFLOW.

SPILLWAY CAPACITY TO TOP OF DAM (EL. 50.4) IS 309 CFS

% CAPACITY OF INFLOW PMF : 6

" OUTFLOW " : 8

" INFLOW 1/2 PMF : 13

" OUTFLOW " : 16



INTERNATIONAL ENGINEERING COMPANY, INC.

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SUCCESS LAKE DAM

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Contract No. 266-04 File No. \_\_\_\_\_  
Designed MP Date 3/5  
Checked D JF Date \_\_\_\_\_

Sheet 3-5

## II. DOWNTSTREAM FAILURE HAZARD

### 1. POTENTIAL IMPACT AREA

THE POTENTIAL IMPACT AREA IS LOCATED 3500 FT DOWNTSTREAM FROM THE DAM

LARGE 5-STORY CONCRETE BUILDING

NEAR BOND STREET, HAS FIRST FLOOR ELEVATION ABOUT 20 FT ABOVE

THE STREAMBED. THERE IS ALSO THE STATE ROUTE 1 BRIDGE LOCATED

ABOUT 1/3 MILES DOWNTSTREAM FROM THE DAM.

### 2. FAILURE OF SUCCESS LAKE DAM.

#### 2. BREACH WIDTH

##### i. HEIGHT OF DAM:

TOP OF DAM EL. 50.4 ; DAM DOWNSTREAM TOE 34.9;  $\therefore H = 15.5 \text{ FT}$

ii. DAM MID-HEIGHT EL. 42.7  $(50.4 - 15.5/2 \approx 42.7)$

iii. APPROXIMATE MID-HEIGHT LENGTH:  $\ell \approx 50 \text{ FT}$  (SPILLWAY LENGTH IS NOT INCLUDED)

\* FROM IECO DRAWINGS

#### iv. BREACH WIDTH (SEE NED-ACE DOWNTSTREAM FAILURE GUIDELINES)

$$W_b = 0.4 \ell = 0.4 \times 50 = 20 \text{ FT}$$

#### b. PEAK FAILURE OUTFLOW ( $Q_{p_f}$ )

ASSUME SURCHARGE AT TOP OF DAM (EL. 50.4)





INTERNATIONAL ENGINEERING COMPANY, INC.

Project

NDIP

Feature

SUCCESS LAKE DAM

Item

Contract No. 2616-C4

Sheet 2-9

File No. \_\_\_\_\_

Designed MP

Date 3/1/81

Checked B

SF

Date \_\_\_\_\_

i. HEIGHT AT TIME OF FAILURE :  $Y_0 = 15.5 \text{ FT}$ ii. SPILLWAY DISCHARGE AT TIME OF FAILURE :  $Q_s = 309 \text{ CFS}$ 

iii. BREACH OUTFLOW :

$$Q_b = \frac{8}{27} w_b \sqrt{g} Y_0^{3/2} = \frac{8}{27} \times 20 \times \sqrt{32.2} \times 15.5^{3/2} = 2052 \text{ CFS}$$

iv. PEAK FAILURE OUTFLOW TO YELLOW MILL CHANNEL TRIBUTARY

$$Q_p = Q_s + Q_b = 309 + 2052 = 2360 \text{ CFS}$$

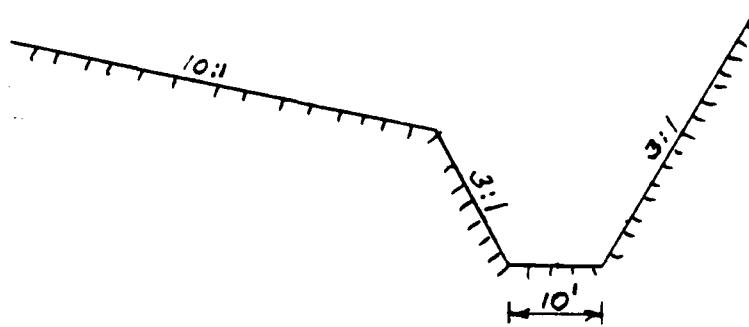
c. FLOOD DEPTH IMMEDIATELY DOWNSTREAM FROM DAM:

$$Y = 0.44 Y_0 = 0.44 \times 15.5 = 6.8 \text{ FT}$$

d. ESTIMATE OF DOWNSTREAM FAILURE CONDITIONS AT POTENTIAL IMPACT AREA  
(SEE NED-ACE GUIDELINES FOR ESTIMATING DOWNSTREAM FAILURE HYDROGRAPHS)

i. REACH OF YELLOW MILL CHANNEL TRIBUTARY BETWEEN DAM AND IMPACT AREA.

VARIES SIGNIFICANTLY IN SECTION. THE FIRST 1500-FOOT-LONG REACH IS APPROXIMATELY SHAPED AS SHOWN ON THE SKETCH BELOW:



CROSS SECTION REACH 1  
THE AVERAGE SLOPE OF THE REACH IS 0.002<sup>(4)</sup>



3-9



INTERNATIONAL ENGINEERING COMPANY, INC.

Project

NDIP

Feature

SUCCESS LAKE DAM

Item

Contract No. 2616-04

Sheet D-10

Designed MP

File No.

Checked B JF

Date 3/11/61

Date

## II SUCCESS LAKE DAM RESERVOIR STORAGE AT TIME OF FAILURE.

STORAGE VOLUME BELOW SPILLWAY CREST APPROXIMATED BY  $\frac{1}{4} \Delta H$ 

$$= \frac{1}{4} \times 12.85 \times 12.1 = 38.9 \text{ AC-FT. SURCHARGE STORAGE TO THE TOP OF THE DAM}$$

(EL. 50.4) is 80.3 AC-FT (SEE STAGE - SURCHARGE CURVE ON P. D-6).

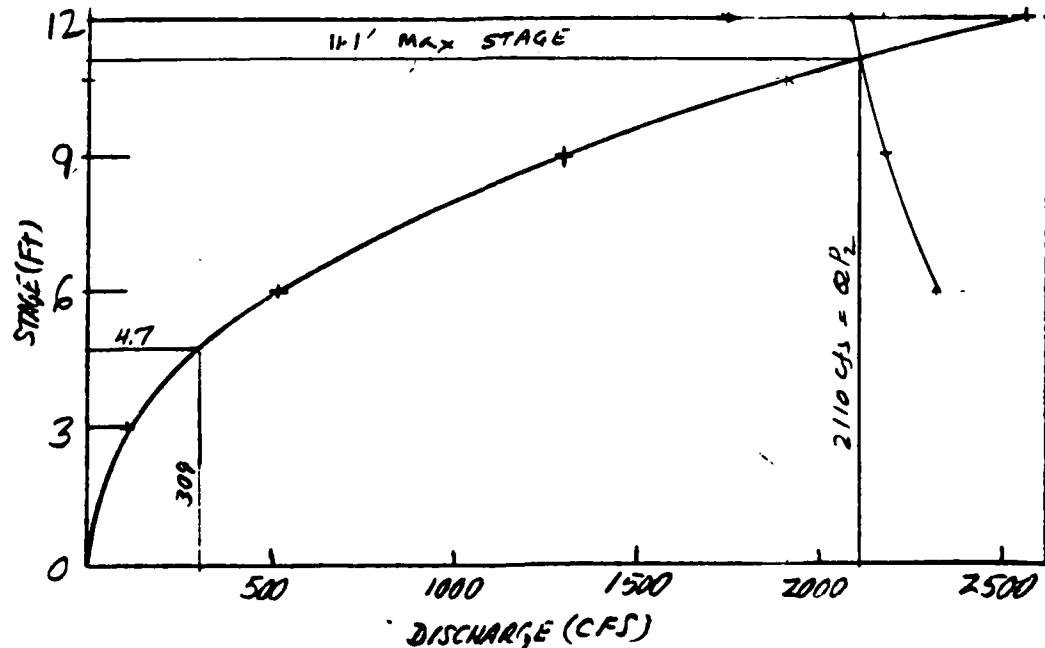
∴ MAXIMUM STORAGE VOLUME OF THE RESERVOIR IS  $38.9 + 80.3 = 119.2 \text{ AC-FT}$ ASSUME  $S_{MAX} = 119 \text{ AC-FT}$ III PEAK INFLOW TO REACH:  $Q_p = 2360 \text{ CFS}$ 

## IV APPROXIMATE STAGE AT POTENTIAL IMPACT AREA FAILURE OF SUCCESS LAKE DAM

REACH L = 3500 FT; n = 0.05; S = 0.002; COMPUTED STAGE - DISCHARGE

CURVE AND STAGE - AREA CURVE FOR THE BROOK SECTION AS SHOWN ON P.D-9

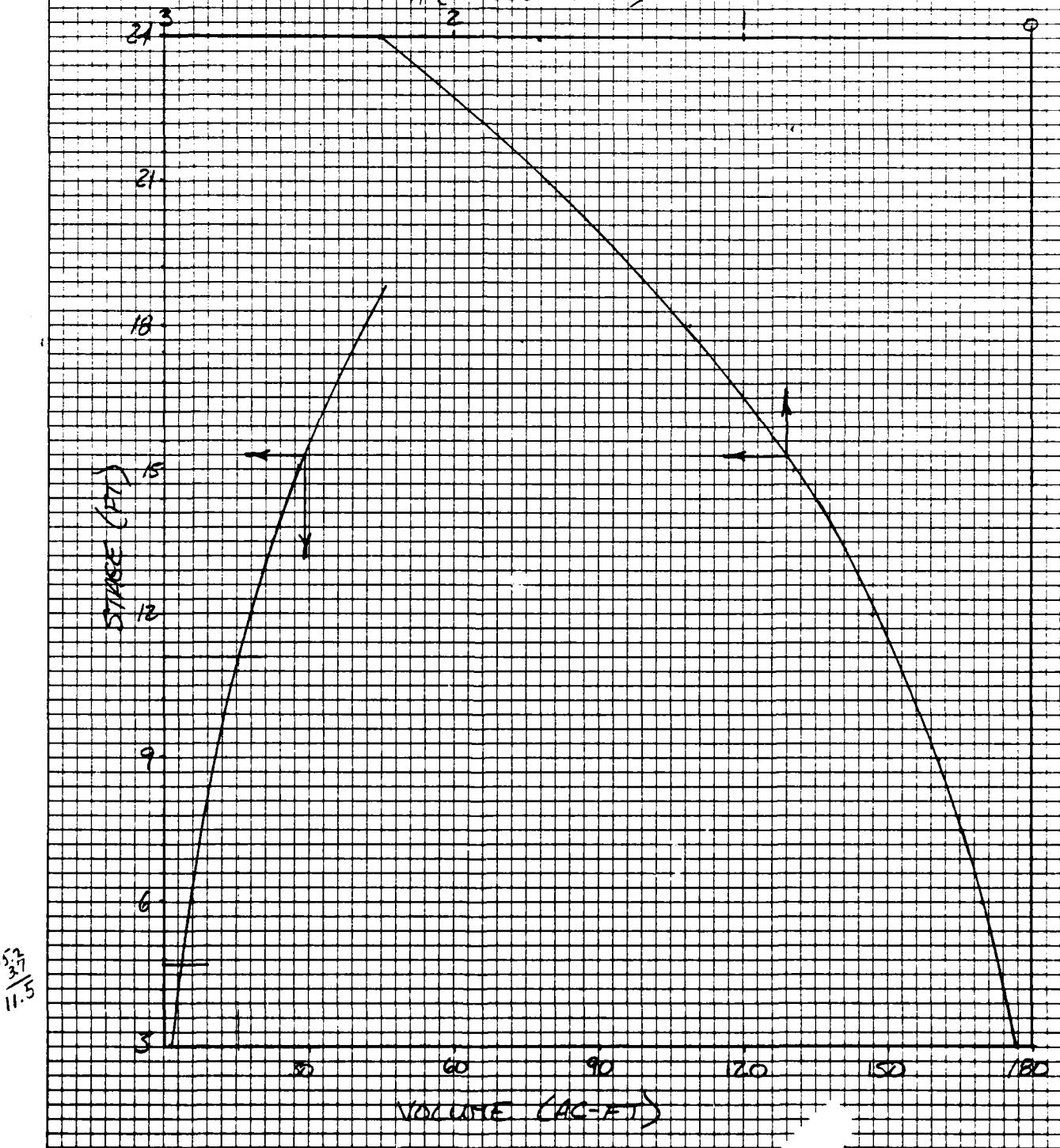
ARE PLOTTED ON P.D-11.

STAGE-DISCHARGE FOR CHANNEL - REACH 1

D-1

AREA CAPACITY CURVE FOR FIRST REACH  
(1500 FEET LONG)

A (in 1000  $\text{ft}^2$ )





INTERNATIONAL ENGINEERING COMPANY, INC.

Project

NDIP

Feature

SUCCESS LAKE DAM

Item

Sheet 0-12

File No.

Date 3/23/71

Contract No. 2616

Designed EHB

Checked A. JF

Date

PRE FAILURE STAGE 4.7FT DISCHARGE 309 CFS

INITIAL VOLUME ABSTRACTED &amp; AC-FT

H	V	$Q_{P2} = 2360 \left(1 - \frac{VOL}{119}\right)$
3	1.7	2406
6	6.0	2320
9	12.9	2183
12	18.1	2080

RISE IN STAGE 11.1 - 4.7 = 6.4'

$$Q_{P2} = 2110 \text{ CFS}$$





INTERNATIONAL ENGINEERING COMPANY, INC.

Project KDIPFeature SUCCESS LAKE DAM

Item \_\_\_\_\_

Contract No. 2616Designed EYBChecked JFSheet D-13

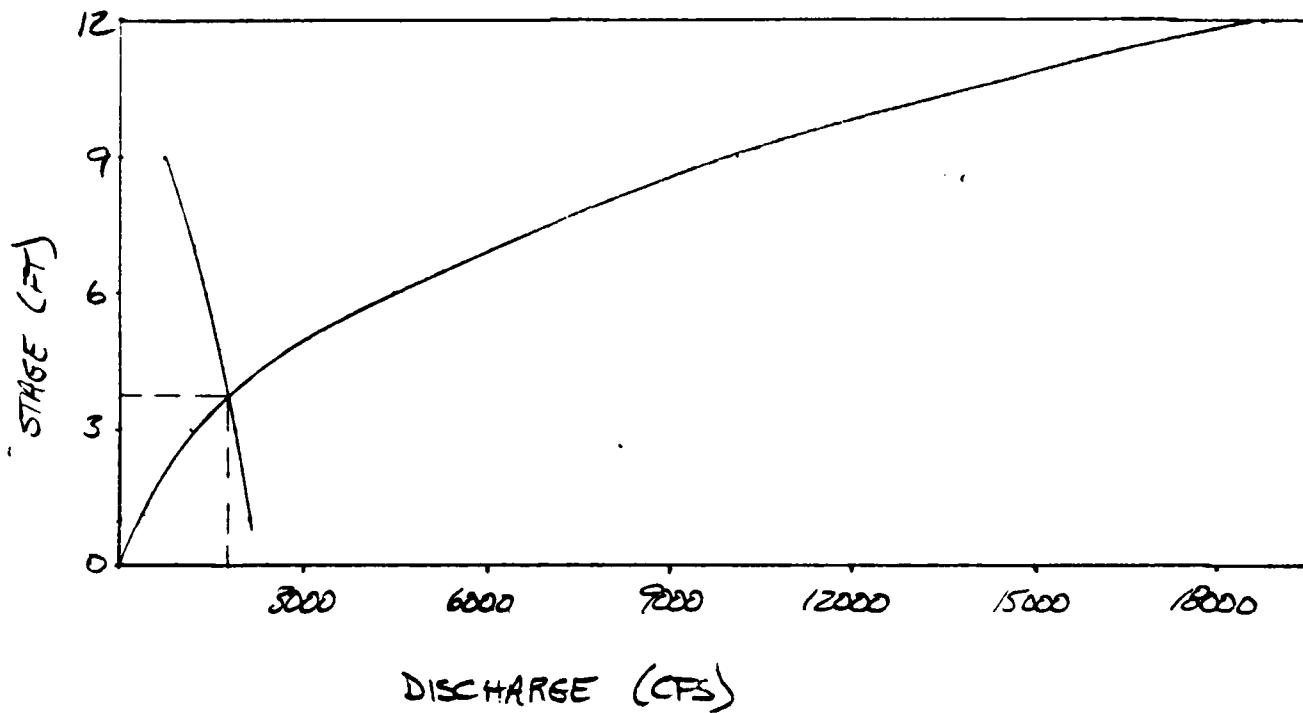
File No. \_\_\_\_\_

Date 3/25/81

Date \_\_\_\_\_

REACH 2:  $L = 1400 \text{ FT}$   $n = 0.05$   $s = 0.002$ 

STAGE DISCHARGE CURVE FOR REACH 2.



PRE FAILURE STAGE 1.0 FT DISCHARGE 309 CFS  
 INITIAL VOLUME ABSTRACTED  $V = 4.4 \text{ AC-FT}$   
 VOLUME ABSTRACTED BY REACH 1  $\Delta V = 11.5 \text{ AC-FT}$   
 POTTING POINTS FOR GRAPHICAL ROUTINE

H	VOL	$Q_{P_2} = 2110 \left(1 - \frac{VOL - 4.4}{119 - 115}\right)$
1	4.4	2110
3	16.06	1881
6	41.07	1390
9	75.04	723

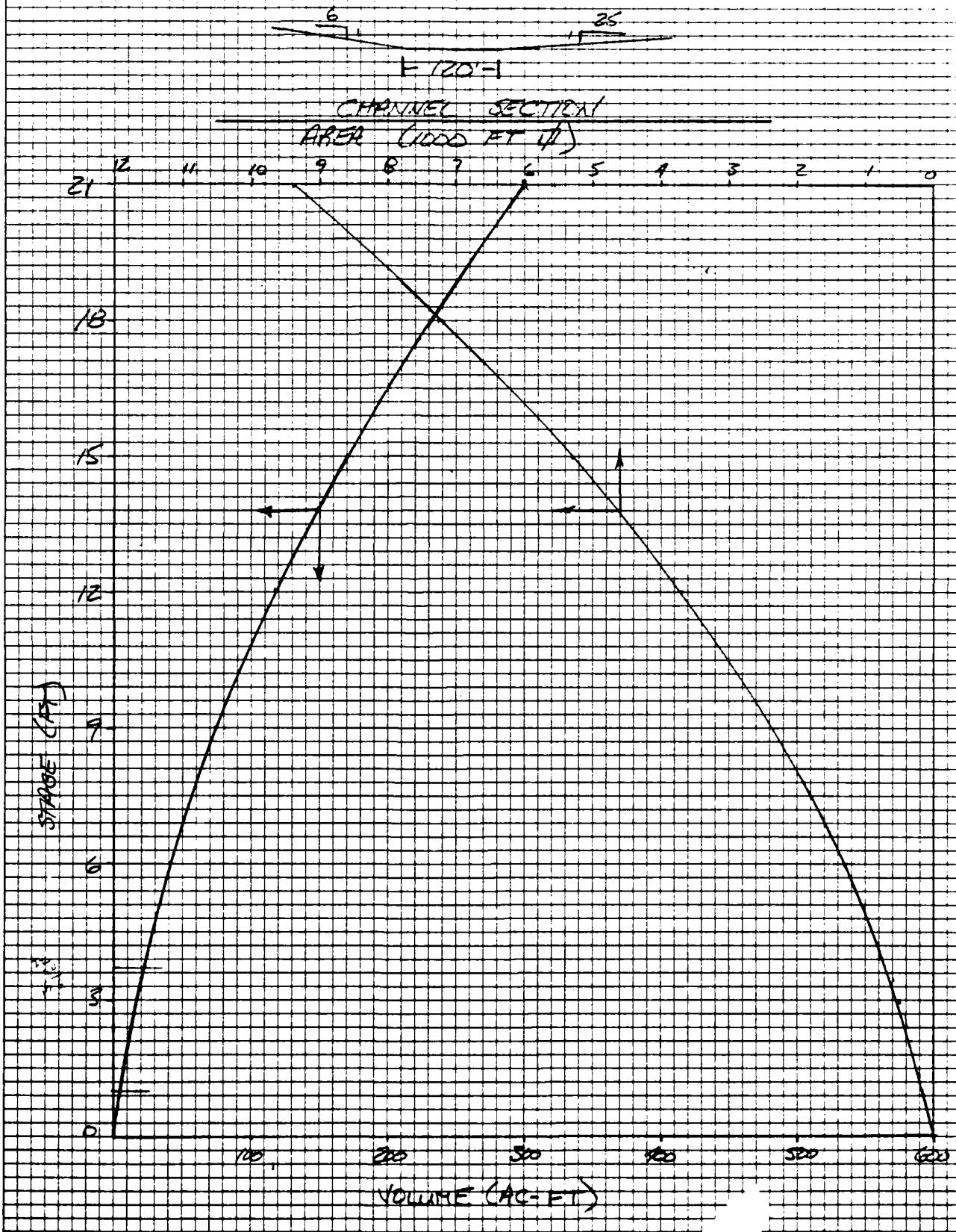
$$Q_{P_2} = 1800 \text{ cfs} \quad H = 3.7 \text{ FT} \quad \Delta H = 2.7 \text{ FT}$$



D-14

M.F.

AREA CAPACITY CURVE FOR SECOND REACH  
(100 FEET LONG)

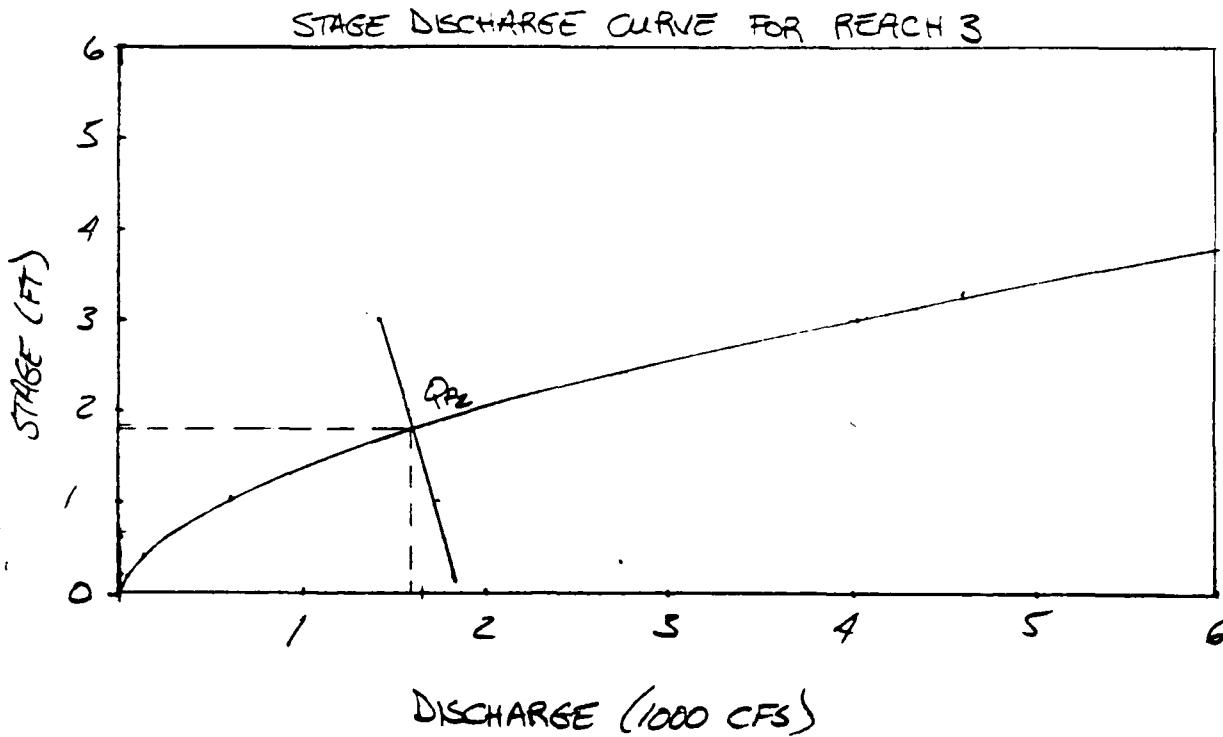




INTERNATIONAL ENGINEERING COMPANY, INC.

Project NDP  
Feature SUCCESS LAKE DAM  
Item \_\_\_\_\_Sheet D-15  
Contract No. 2616  
File No. \_\_\_\_\_  
Designed EHR  
Date 3/23/81  
Checked by JF  
Date \_\_\_\_\_

REACH 3:  $L = 600 \text{ FT}$   $n = 0.05$   $s = 0.002$



PREFAILURE STAGE  $\approx 0.7 \text{ FT}$  DISCHARGE  $309 \text{ CFS}$

INITIAL VOLUME ABSTRACTED  $\approx 3 \text{ AC-FT}$

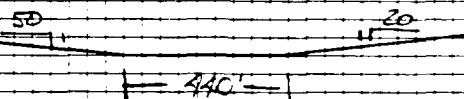
$$H \quad VOL \quad Q_{P_2} = 1800 \left( 1 - \frac{VOL^3}{119-17.5} \right)$$

0.2	1.2	1836
0.6	3.8	1784
1.0	6.5	1730
1.4	9.1	1672
2.0	14.0	1580
3.0	22.5	1410



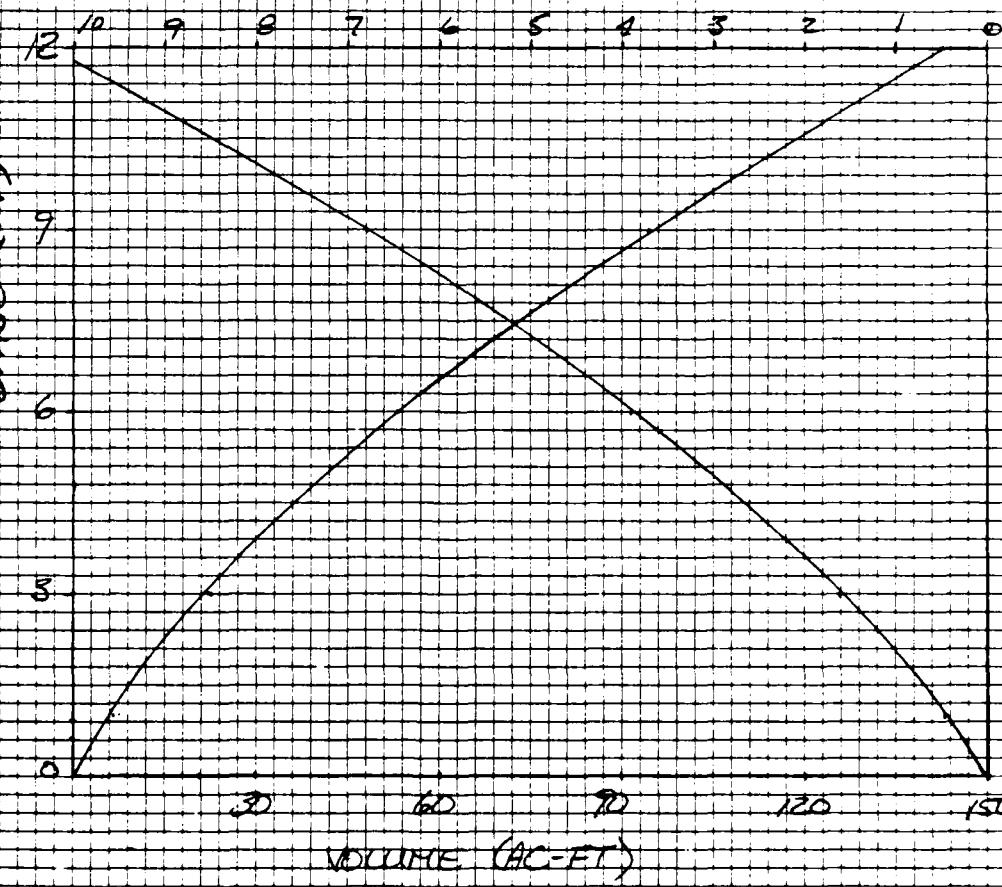
L.J.F D-16

AREA CAPACITY CURVE F.P. THIRD  
REACH ( $L = 600\text{FT}$ )



CHANNEL SECTION  
THIRD REACH

AREA (1000 FT  $\phi$ )





INTERNATIONAL ENGINEERING COMPANY, INC.

Project NDIP Contract No. 2616  
Feature SUCCESS LAKE DAM Designed EHR  
Item \_\_\_\_\_ Checked A.JF

Sheet D-17

File No. \_\_\_\_\_

Date 3/23/81

Date \_\_\_\_\_

$$Q_{P_2} = 1620 \text{ CFS} \quad H = 1.8 \text{ FT}$$

$$\text{RISE IN STAGE } \Delta H = 1.8 - 0.7 = 1.1 \text{ FT}$$

III. THE RISE IN STAGE WITHIN THE FIRST REACH  
WILL NOT EFFECT THE STRUCTURE IMMEDIATELY U/S  
FROM THE DAM (1<sup>ST</sup> FLOOR EL ± 20FT ABOVE STREAM BED)  
THE RISE IN STAGE WITHIN THE THIRD REACH WILL  
HAVE LITTLE OR NO EFFECT ON THE STRUCTURES NEAR  
THE STREAM.



8

AD-A142 830

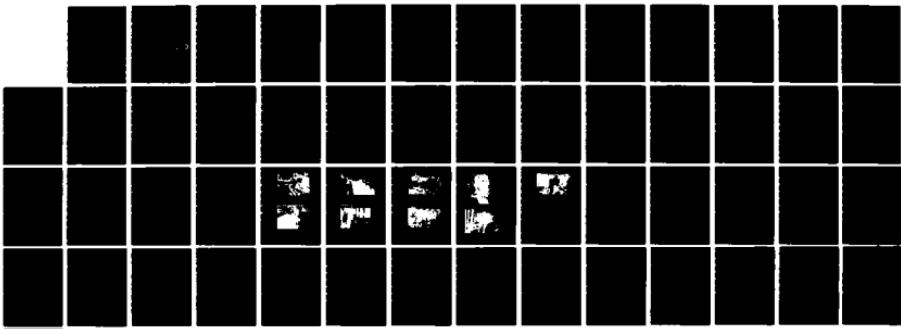
NATIONAL PROGRAM FOR INSPECTION OF NON-FEDERAL DAMS  
SUCCESS LAKE DAM (CT. (U) CORPS OF ENGINEERS WALTHAM MA  
NEW ENGLAND DIV MAY 81

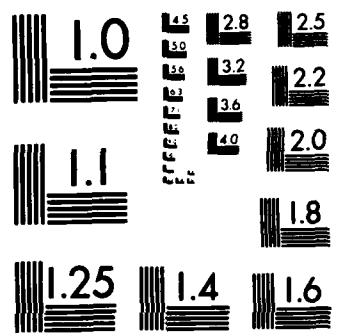
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UNCLASSIFIED

F/G 13/13

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MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

AD-A142 830

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER CT 00079	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Success Lake Dam Conn. Coastal Basin, Bridgeport, Conn. NATIONAL PROGRAM FOR INSPECTION OF NON-FEDERAL DAMS		5. TYPE OF REPORT & PERIOD COVERED INSPECTION REPORT
7. AUTHOR(s) U.S. ARMY CORPS OF ENGINEERS NEW ENGLAND DIVISION		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS DEPT. OF THE ARMY, CORPS OF ENGINEERS NEW ENGLAND DIVISION, NEDED 424 TRAPELO ROAD, WALTHAM, MA. 02254		12. REPORT DATE May 1981
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		13. NUMBER OF PAGES 50
		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) APPROVAL FOR PUBLIC RELEASE: DISTRIBUTION UNLIMITED		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES Cover program reads: Phase I Inspection Report, National Dam Inspection Program; however, the official title of the program is: National Program for Inspection of Non-Federal Dams; use cover date for date of report.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) DAMS, INSPECTION, DAM SAFETY, Success Lake Dam Conn. Coastal Basin Bridgeport, Conn.		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The Success Lake Dam, constructed in 1875, is a 132 ft. long, 17 ft. high structure composed of two earthfill embankments and a central 33 ft. long broad crested spillway. The original timber spillway decking has since been capped with concrete. There is a small single land bridge, across the overflow spillway section. Flow over the spillway is channeled through five 4 ft. wide, 2 ft. high openings, and one 3.3 ft. wide, 2 ft. high, opening formed by the bridge piers. The upstream concrete face of the spillway has a slope of approx. 2H:1V and the masonry downstream face is vertical.		

## SUCCESS LAKE DAM

CT 00079

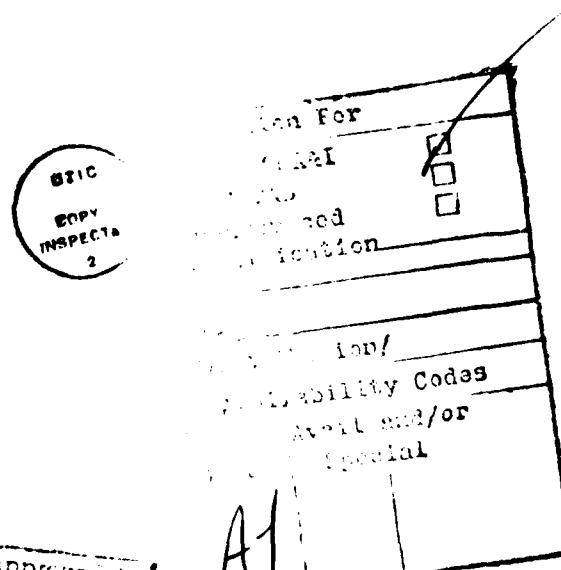
## **CONNECTICUT COASTAL BASIN**

**BRIDGEPORT, CONNECTICUT**

## PHASE I INSPECTION REPORT

## NATIONAL DAM INSPECTION PROGRAM

MAY 1981



This document has been approved  
for public release and sale; its  
distribution is unlimited.

84 06 20 00

CONSULTING  
ENGINEERS

**INTERNATIONAL ENGINEERING COMPANY, INC.**  
A MORRISON-KNUDSEN COMPANY

EASTERN DISTRICT OFFICE  
777 POST ROAD DARIEN CONNECTICUT 06820  
PHONE 203 655-3345

11410  
2616-110

May 7, 1981

Mr. E. P. Gould  
Project Management Branch  
Department of the Army  
New England Division  
Corps of Engineers  
424 Trapelo Road  
Waltham, Massachusetts 02154

Reference: Contract No. DACW33-81-C-0015  
Inspection and Evaluation of Non-Federal Dams  
FY-81, Southwestern Connecticut

Dear Mr. Gould:

The inspection of Success Lake Dam and subsequent hydrologic-hydraulic investigation revealed that the dam should be classified as having a low hazard potential. The following is an abbreviated Phase I Inspection report to substantiate this classification.

Sincerely,

*Reynold A. Hokenson*

Reynold A. Hokenson, P. E.  
Project Manager

RAH:mem

Enclosures

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ANALYTICAL DAM INSPECTION PROGRAM

PHASE I INSPECTION REPORT

Identification No: CT 00079

Name of Dam: Success Lake Dam

Town: Bridgeport

County and State: Fairfield, Connecticut

Stream: Yellow Mill Channel

Dates of Inspection: February 5 and 19, 1981

BRIEF ASSESSMENT

The Success Lake Dam impounds Success Lake on the Yellow Mill Channel tributary in Bridgeport, Fairfield County, Connecticut. The structure is currently owned by Remington Arms Company, Inc., 939 Barnum Avenue, Bridgeport, Connecticut. The operation of the facility is the responsibility of Robert H. Gruss, Plant Engineer, Remington Arms Co., Inc., (203) 333-1112. Currently, the impoundment is maintained for aesthetics and wildlife conservation.

The Success Lake Dam, constructed in 1875, is a 132-foot-long, 17-foot-high structure composed of two earthfill embankments and a central 33-foot-long broad crested spillway. The original timber spillway decking has since been capped with concrete. There is a small single land bridge, across the overflow spillway section (Photo 1). Flow over the spillway is channeled through five 4-foot-wide, 2-foot-high openings, and one 3.3-foot-wide, 2-foot-high, opening formed by the bridge piers. The upstream concrete face of the spillway has a slope of approximately 2H:1V and the masonry downstream face is vertical. The downstream slopes of the two-side embankments are formed by vertical stone retaining walls. The upstream slopes also appeared to be vertical stone retaining walls, however, these areas were, for the most part, concealed beneath the water surface and accumulated sediments (Photos 2 and 3).

Two cast iron conduits pass through the earthfill embankment at the right abutment of the dam and provide additional outlets from the impoundment. A 14 inch diameter conduit exits the dam near its base approximately 12 feet from the right side of the spillway. Discharges from this conduit are regulated by a hand operated valve which is housed in a small masonry structure (Photo 9). The second conduit is 8 inches in diameter and emerges from the right embankment, approximately 5 feet below the top of the dam and about 25 feet from the spillway (Photo 7). This conduit extends 126 feet downstream to a small brick structure where, at one time, it provided water for the generation of steam (Photo 8). The brick structure formerly housed equipment for the generation and distribution of steam to the various industrial processes that were performed by Remington Arms Company, Inc., in the 1940's. This equipment was removed from the site and the building was converted to an employee locker room. The 8-inch conduit leading to this building, though deteriorated, is still intact.

Visual inspection of the site indicated that the dam is in poor condition. The inspection revealed the following: deterioration of the vertical downstream face of the spillway, cracked and missing portions of the concrete spillway crest along the downstream edge (Photo 4), cracks along the upstream and downstream interfaces of the spillway and abutments, exposed aggregate on the concrete spillway cap, seepage along the toe of the left embankment has resulted in a 20-foot by 30-foot marshy area approximately 40 feet from the dam, and a potentially inoperable low-level outlet. The seepage beneath the spillway, described in the inspection report submitted by William P. Sanders of the State of Connecticut Water Resource Commission on July 22, 1964 (see Correspondence), was not confirmed during the inspections conducted by IECO on February 2 and 19, 1981. During these inspections, an accumulation of rocks at the base of the spillway, ice formations on the downstream face of the spillway and particularly water flowing over the spillway made it impossible to examine this portion of the dam closely (Photos 5 and 6). Water was observed draining vertically through cracks in the concrete cap near the left upstream spillway abutment, but no corresponding flow of discharge was noted on the downstream

face of the spillway. In addition, localized outward movement of the stone retaining wall and the concrete spillway cap were also found in the vicinity of the left spillway abutment. The effected area is approximately 7 feet wide, but the movement has been slight and is a local condition not threatening the dam.

The Success Lake Dam has a maximum potential storage capacity of 119 acre-feet (ac-ft) and is approximately 17 feet in height. Since the dam falls within the Corp's criteria for the small size category based on storage (between 50 and 1,000 ac-ft), the dam is considered to be SMALL in size. The dam breach analysis was conducted in accordance with the "Rule of Thumb Guidance for Estimating Downstream Dam Failure Hydrographs", dated April 1978, and the potential impact area was defined. Failure of the dam would cause the water surface within the streambed immediately downstream of the dam to rise from 4.7 feet at a prefailure outflow of 310 cfs to 11.1 feet at an outflow of 2,360 cfs. The first floor of the brick structure located approximately 130 feet downstream from the dam is more than 20 feet above the streambed, and this will not be effected by the flood wave. The only remaining other structures adjacent to the Yellow Mill Channel are located 3,500 feet downstream from the dam. These will sustain little or no damage since the water surface within this reach will rise only 1.8 feet above the streambed. Since failure of the dam will cause little or no property damage and no loss of life, the dam has been classified as having a LOW hazard potential.

LOCATION MAP  
CONNECTICUT  
SCALE 1:4000

0 2000 4000 FEET

SUCCESS LAKE DAM

CONNECTICUT  
QUADRANGLE LOCATION

USGS QUADRANGLE  
BRIDGEPORT 1970

**APPENDIX A**

**INSPECTION CHECKLIST**

VISUAL INSPECTION CHECK LIST  
PARTY ORGANIZATION

PROJECT Success Lake Dam

DATE 02/5 & 19/81

TIME 10:00 a.m.

WEATHER Sunny, Cold

W.S. ELEV. 47.1

PARTY:

INITIALS:

1. Jeffrey T. Klaucke	JK
2. Myron B. Petrovsky	MP
3. Ernst H. Buggisch	EB
4. Paul Archer	PA
5. Harold Farnham	HF (Matthews Associates)

PROJECT FEATURE:

INSPECTED BY:

1. Dam	JK, MP, EB, PA
2. Intake Channel	JK, MP
3. Valvehouse	JK, HF, MP
4. Powerhouse Conduit	HF, JK, MP
5. Low Level Outlet	HF, JK, MP
6. Low level Outlet Channel	JK, MP, EB, PA
7. Spillway	JK, MP, EB
8. Bridge	JK, PA, EB

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam

DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Dam

NAME: JK, MP, EB, PA

AREA EVALUATED	CONDITION
<u>DAM EMBANKMENT</u>	
Crest Elevation	47.0
Current Pool Elevation	47.1
Maximum Impoundment to Date	Approximately 50.0
Surface Cracks	None
Pavement Condition	Good
Movement or Settlement of Crest	None
Lateral Movement	Local movement on upstream face near left spillway abutment.
Vertical Alignment	Good
Horizontal Alignment	Good
Condition at Abutment and at Concrete Structures	Cracks along U/S and D/S interfaces with spillway.
Indications of Movement of Structural Items on Slopes	Minor bulging of U/S and D/S retaining walls.
Trespassing on Slopes	None.
Sloughing or Erosion	None
Rock Slope Protection	The exposed U/S walls were irregular and missing stones.
Unusual Movement or Cracking at or near Toes	None
Unusual Embankment or Downstream Seepage	Wet area at D/S toe on the left bank. Seepage noted through valvehouse.
Piping or Boils	Possible piping along low level outlet conduit.

## PERIODIC INSPECTION CHECK LIST

PROJECT: <u>Success Lake Dam</u>	DATE: <u>02/5 &amp; 19/81</u>
PROJECT FEATURE: <u>Dam (Continued)</u>	NAME: <u>JK, MF, EB, PA</u>
AREA EVALUATED	CONDITION
Foundation Drainage Features	Unknown
Toe Drains	Unknown
Instrumentation System	None

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake DamDATE: 02/5 & 19/81PROJECT FEATURE: Intake ChannelNAME: JK, MP

AREA EVALUATED	CONDITION
<u>OUTLETS WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE</u>	
a. Approach Channel	Success Lake
Slope Conditions  Bottom Conditions  Rock Slides or Falls  Log Boom  Debris  Condition of Concrete Lining  Drains or Weep Holes	
b. Intake Structure	No structure visible above current pool level.
Condition of Concrete  Stop Logs and Slots	

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake DamDATE: 02/5 & 19/81PROJECT FEATURE: ValvehouseNAME: JK, HF, MP

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - CONTROL TOWER</u>	
a. Concrete and Structural	
General Condition	Fair, wooden roof rotted.
Condition of Joints	Good
Spalling	None
Visible Reinforcing	None
Rusting or Staining of Concrete	Near crack in valvehouse wall
Any Seepage or Efflorescence	Seepage noted through crack in valvehouse wall.
Joint Alignment	Good
Unusual Seepage or Leaks in Gate Chamber	None
Cracks	Right wall of valvehouse
Rusting or Corrosion of Steel	Exposed portion of low level outlet conduit.
b. Mechanical and Electrical	
Air Vents	
Float Wells	
Crane Hoist	
Elevator	
Hydraulic System	
Mechanical Valve	Not tested at owner's request
Emergency Gates	
Lightning Protection System	
Emergency Power System	
Wiring and Lighting System	

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam	DATE: 02/5 & 19/81
PROJECT FEATURE: Low level Outlet	NAME: HF, JK, MP
AREA EVALUATED	CONDITION
<u>OUTLET WORKS - TRANSITION AND CONDUIT</u>	
General Condition of Conduit	Fair
Rust or Staining on Conduit	Superficial rust on exposed conduit.
Spalling	N/A
Erosion or Cavitation	None
Cracking	None
Alignment of Monoliths	N/A
Alignment of Joints	N/A
Numbering of Monoliths	N/A
<u>Note:</u> Only a small portion of the cast iron conduit (approximately 8 in.) was visible.	

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam

DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Low Level Outlet Channel

NAME: JK, MP, EB, PA

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL</u>	
General Condition of Concrete	N/A
Rust or Staining	
Spalling	
Erosion or Cavitation	
Visible Reinforcing	
Any Seepage or Efflorescence	
Condition at Joints	
Drain holes	
Channel	
Loose Rock or Trees Overhanging Channel	Large rocks and 5 to 20 in. diameter trees were found immediately D/S of the outlet and adjacent to the spillway discharge channel.
Condition of Discharge Channel	Large rocks have accumulated on the channel floor.

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam

DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Spillway

NAME: JK, HF, EB

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS</u>	
a. Approach Channel	Success Lake
General Condition	
Loose Rock Overhanging Channel	
Trees Overhanging Channel	
Floor of Approach Channel	
b. Weir and Training Walls	
General Condition of Masonry	Loose stones in retaining walls, some stones missing and wall movements noted near spillway.
Rust or Staining	None
Spalling of spillway concrete cap	Near downstream edge of spillway weir.
Any Visible Reinforcing	None
Any Seepage	Some vertical drainage into dam through cracks in the spillway cap.
Drain Holes	None
c. Discharge Channel	
General Condition	Fair
Loose Rock Overhanging Channel	Loose rocks from downstream walls of spillway have accumulated in discharge channel.
Trees Overhanging Channel	Large tree on right bank between valvehouse and spillway.
Floor of Channel	Strewn with large rocks.
Other Obstructions	None

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake DamDATE: 02/5 & 19/81PROJECT FEATURE: BridgeNAME: JK, PA, EB

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - BRIDGE</u>	
a. Super Structure Bearings	N/A
Anchor Bolts	N/A
Bridge Seat	N/A
Longitudinal Members	N/A
Under Side of Deck	Good
Secondary Bracing	None
Deck	Good
Drainage System	All 3 inch diameter drains in curbs were free of obstructions.
Railings	Good
Expansion Joints	None
Paint	N/A
b. Piers	
General Condition of Concrete	Good
Alignment of Abutment	
Approach to Bridge	
Condition of Seat & Backwall	<u>Note:</u> The bridge is supported 2 feet above the spillway by 4 concrete piers that are founded on the spillway.

## PERIODIC INSPECTION CHECK LIST

PROJECT: Success Lake Dam DATE: 02/5 &amp; 19/81

PROJECT FEATURE: Powerhouse Conduit NAME: JK, HF, MP

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - CONTROL TOWER</u>	
a. Concrete and Structural	
General Condition	N/A
Condition of Joints	
Spalling	
Visible Reinforcing	
Rusting or Staining of Concrete	
Any Seepage or Efflorescence	
Joint Alignment	
Unusual Seepage or Leaks in Gate Chamber	
Cracks	
Rusting or Corrosion of Steel	
b. Mechanical and Electrical	
Air Vents	
Float Wells	
Crane Hoist	
Elevator	
Hydraulic System	
Mechanical Valve	Valve inoperable, conduit has not been used since the 1940's.
Emergency Gates	
Lightning Protection System	
Emergency Power System	
Wiring and Lighting System	

APPENDIX B

ENGINEERING DATA

SUMMARY OF DATA AND CORRESPONDENCE

<u>DATE</u>	<u>TO</u>	<u>FROM</u>	<u>SUBJECT</u>	<u>PAGE</u>
			Water Resources Inventory Data	B-2
6/7/66	Mr. W.H. O'Brien III Water Resources Commission State of Connecticut	Joseph W. Cone Civil Engineer	Inspection	B-3
10/9/64	State of Connecticut Water Resources Commission State of Connecticut	J. P. Barry Works Engineer Remington Arms Company, Inc.	Verification upon completion of suggested repairs	B-6
7/22/64	H.M. Pierce Jr. Plant Manager Remington Arms Company, Inc.	William P. Sander Engineer-Geologist State of Connecticut	Suggested spillway repairs	B-7
			COE Inventory Data	B-8

No. \_\_\_\_\_

WATER RESOURCES UNIT  
SUPERVISION OF DAMS  
INVENTORY DATA

Inventoried  
By \_\_\_\_\_

Lat:  $41^{\circ}$  12.3'

Date \_\_\_\_\_

Long:  $73^{\circ}$  9.9'

Name of Dam or Pond SUCCESS LAKE

Code No. \_\_\_\_\_

Nearest Street Location Huntington Turnpike

Town Bridgeport

U.S.G.S. Quad. Bridgeport

Name of Stream Unnamed

Owner Remington Arms Company, Inc.

Address Barnum Avenue

Bridgeport, CT

Pond Used For Fire Protection Drainage Area 2.43 sq. mi.

Dimensions of Pond: Width 700' Length 1100' Area 18.3 ac.

Total Length of Dam 125' Length of Spillway 35'

Location of Spillway Center of dam

Height of Pond Above Stream Bed 15'

Height of Embankment Above Spillway 3'

Type of Spillway Construction Concrete cap

Type of Dike Construction Masonry

Downstream Conditions Bridgeport

Summary of File Data \_\_\_\_\_

Remarks \_\_\_\_\_

Would Failure Cause Damage? \_\_\_\_\_ Class \_\_\_\_\_

NEW YORK LICENSE 4755  
CONNECTICUT REGISTRATION 4

JOSEPH W. CONE  
CIVIL ENGINEER  
124 HAVEMEYER PLACE  
GREENWICH, CONNECTICUT  
06830

STATE TOWNSEND 9-2152  
TOWNSEND REED & CO.  
COMMISSION  
RECEIVED

June 7, 1966

JUN 10 1966

ANSWERED  
REFERRED  
FILED

Mr. William H. O'Brien III  
Water Resources Commission  
State Office Building  
Hartford 15, Conn.

Re: Dam #46 Stillman Pond-Bdpt.  
A.V.D SUCCESS LAKE D.A.M

Dear Mr. O'Brien:

As requested, I have inspected the Stillman Pond Dam and the tributary watershed. Also permission was obtained from Remington Arms office to inspect Success Lake Dam, being escorted by one of their guards, since the condition of this dam is involved with Stillman.

	Success	Stillman
Watershed	2.28 sq.mi.	3.44 sq. mi.
Peak Q pres 100 yr	1250 cfs	1890 cfs
" " 2000 AD 400 yr	4370 "	5130 "

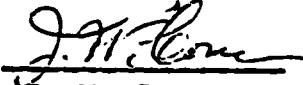
Both dams are solidly constructed and, in my opinion, will not fail but both will be overtopped in the future. Both have very low headroom, Success 6 openings averaging 4'x2'; openings were not measured at Stillman, it was evident that dam is safe although it will be overtopped.

Tracks serving the G.E. Plant will be flooded in the future during a severe storm due to channel of inadequate capacity.

Copies of work sheets, three photos and map of watersheds are enclosed. See Lake Forest for more applicable data.

My recommendation is that your office suggest to Remington Arms and General Electric that there be a standing order that their maintenance men see to it that openings at dams be kept clear of debris during heavy storms, this to reduce frequency of overtopping.

Very truly yours,

  
J. W. Cone

JWC/dr  
Enc: 6

Foothills Grade

FOREST  $\frac{125 \text{ Ac}}{25 \text{ yr. return}}$  —  $1.445 \text{ sp. mi}$   $n = 1.2$

(cont'd)  $Q_{\text{Peak}} = 850 \text{ cfs}$  Wint. end 1950

Entire sheet developing rapidly. Rolling terrain.

$Q_{\text{present 25 yr}} = RF \times LF \times FF \times Q$

$$= 1 \times 0.8 \times 1 \times 850 = 680 \text{ cfs} \quad 0.73$$

$$Q_{\text{" 100 yr}} = 1 \times 0.8 \times 1.8 \times 850 = 1220 \quad 1.22$$

$$Q_{\text{" 400 yr}} = 1 \times 0.8 \times 3.8 \times 850 = 2580 \quad 2.8$$

$$\text{" 2000 AD"} = 1 \times 1.0 \times 3.8 \times 850 = 3240 \quad 3.5$$

Compare 3240 with 1955 Floods. 1.5 sp. mi. on  $Q = 5000 \text{ cfs} = 4150 \text{ ft}^3/\text{s}$   
 $= 6000 \text{ m}^3/\text{s}$  on 1.445

SUCCESS  $1460 \text{ Ac} = 2.28 \text{ sp. mi}$

Entire area developing rapidly except 132 Ac occupied by Pct. Forest.  
 Rolling terrain rather flat

Chart B  $Q = 1150 \text{ cfs}$

$Q_{\text{present 25 yr}} = RF \times LF \times FF \times Q$

$$= 1 \times 0.5 \times 1 \times 1150 = 675 \text{ cfs} \quad 0.47$$

$$\text{" 100 } = 1 \times 0.5 \times 1.8 \times 1150 \quad 1250 \quad 0.55$$

$$\text{" 400 } = 1 \times 0.5 \times 3.8 \times 1150 \quad 2220 \quad 1.3$$

$$\text{" 2000 AD"} = 1 \times 1.0 \times 3.8 \times 1150 \quad 4370 \quad 3.0$$

Provided Pump Tires Controls. Large area.

STILLING  $2200 \text{ Ac}$   $\frac{3445 \text{ sq. mi.}}{25 \text{ yr. return}}$  Chart B  $Q = 1500$

(cont'd)  
455

$Q_{\text{present 25 yr}} = RF \times LF \times FF \times Q$

$$= 1 \times 0.7 \times 1 \times 1500 = 1050 \quad 0.48 \text{ cfs/ha}$$

$$\text{" 100 } = 1 \times 0.7 \times 1.8 \times 1500 \quad 1890 \quad 0.86$$

$$\text{" 400 } = 1 \times 0.7 \times 3.8 \times 1500 \quad 4000 \quad 1.8$$

$$\text{" 2000 AD"} = 1 \times 0.9 \times 3.8 \times 1500 \quad 5130 \quad 2.3$$

Provided from Areas of G.I. do not develop 330 Ac.



*Remington*  
OPIUM

*PETERS*  
OPIUM

# REMINGTON ARMS COMPANY, INC.

MANUFACTURERS OF  
SPORTING FIREARMS, AMMUNITION

TRAPS

TARGETS

PETERS CARTRIDGE DIVISION

BRIDGEPORT, CONN

TRAPS AND TARGETS, FINDLAY, OHIO

CABLE - HARTLEY, BRIDGEPORT

- ALL CODES -

ARMS AND CARTRIDGE POWERED TOOLS  
ILION, N. Y.

AMMUNITION, BRIDGEPORT, CONN.  
POWER TOOLS, PARK FOREST, ILL.

POWER TOOLS

BRIDGEPORT 2, CONNECTICUT

October 9, 1964

SUCCESS LAKE DAM  
BRIDGEPORT

State of Connecticut  
Water Resources Commission  
State Office Building  
Hartford 15, Connecticut

Attention Mr. William P. Sander, Engineer-Geologist

Gentlemen:

Reference - Your letter of July 22, 1964

The leakage under the spillway is a condition we are aware of and have been checking periodically. There is no apparent increase in the water flow over the past ten years and we, therefore, feel this is not a condition to cause concern. The massive construction of this dam should be adequate if the leaks do not become larger, or general deterioration set in.

We have a periodic inspection set up whereby the quantity of water leaking is measured and checked against previous findings. Any increase will be readily recognized and prompt remedial action will be taken.

The trees specified in your report have been removed.

Very truly yours,

REMININGTON ARMS COMPANY, INC.  
H.M. PIERCE, JR., WORKS MANAGER

*J. P. Barry*  
J. P. Barry  
Works Engineer

JPB:O'L

STATE WATER RESOURCES COMMISSION	
RECEIVED	
OCT 13 1964	
ANSWERED _____	B-6
REFERRED _____	
FILED _____	

July 22, 1964

Mr. H. M. Pierce, Jr., Plant Manager  
Remington Arms Company, Inc.  
Barnum Avenue  
Bridgeport, Connecticut

Dear Sir:

The Water Resources Commission has recently completed an inventory of all the dams in the Town of Bridgeport.

During the inventory, the dam forming Success Lake was inspected and was found to be in need of repair. At the date of the inspection, all stream flow was through leakage under the spillway. In addition, the trees which are growing on the dam should be removed. These points are not critical at the present time but represent a condition which could lead to failure of the dam.

We would appreciate hearing what plans you have to place this structure in a safe condition.

Very truly yours,

William P. Sander  
Engineer - Geologist

WPS:js

APPENDIX H - LAMAS INPUT FILE (A)

STATE NUMBER	COUNTY	STATE NUMBER	COUNTY	STATE NUMBER	COUNTY
C1	10	NDU	C1	001	04

SUCCESS LAKE DAM

FURNAR NAME		NAME OF IMPOUNDMENT	
(1) (2)		(3) (4)	

SUCCESS LAKE

RIVER OR STREAM		NEAREST DOWNSTREAM CITY-TOWN-VILLAGE	
(5) (6)		(7) (8)	

RED-YELLOW MILL CHANNEL

MILL MULL

TYPE OF DAM		YEAR COMPLETED	PURPOSES	HYDRO-ELECTRIC	IMPOUNDING CAPACITIES
CR	1875	0		MAX. HEAD M.F.T. F.C.	MAXIMUM HEAD F.C. F.C.

1875

0

18

17

124

109

NEW

REMARKS

20=ESTIMATE 22=ESTIMATE

DIS	SPILLWAY	MAXIMUM	VOLUME	POWER CAPACITY	NAVIGATION LOCKS
125	STRAIGHT TYPE	55	OF DAY (CFS)	INSTALLED POWER	NO

125

55

(1) (2)

(3) (4)

(5) (6)

(7) (8)

(9) (10)

(11) (12)

(13) (14)

(15) (16)

(17) (18)

(19) (20)

(21) (22)

(23) (24)

(25) (26)

(27) (28)

(29) (30)

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(33) (34)

(35) (36)

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(67) (68)

(69) (70)

(71) (72)

(73) (74)

(75) (76)

(77) (78)

(79) (80)

(81) (82)

(83) (84)

(85) (86)

(87) (88)

(89) (90)

Letter approx. time & date  
2 weeks

Call to reserve clearance. On days notice.

Bob Gross Ext 1316.

REPORT CONTROL SYMBOL  
DAEN-CRM-17

**APPENDIX C**

**PHOTOGRAPHS**

— SUCCESS LAKE —

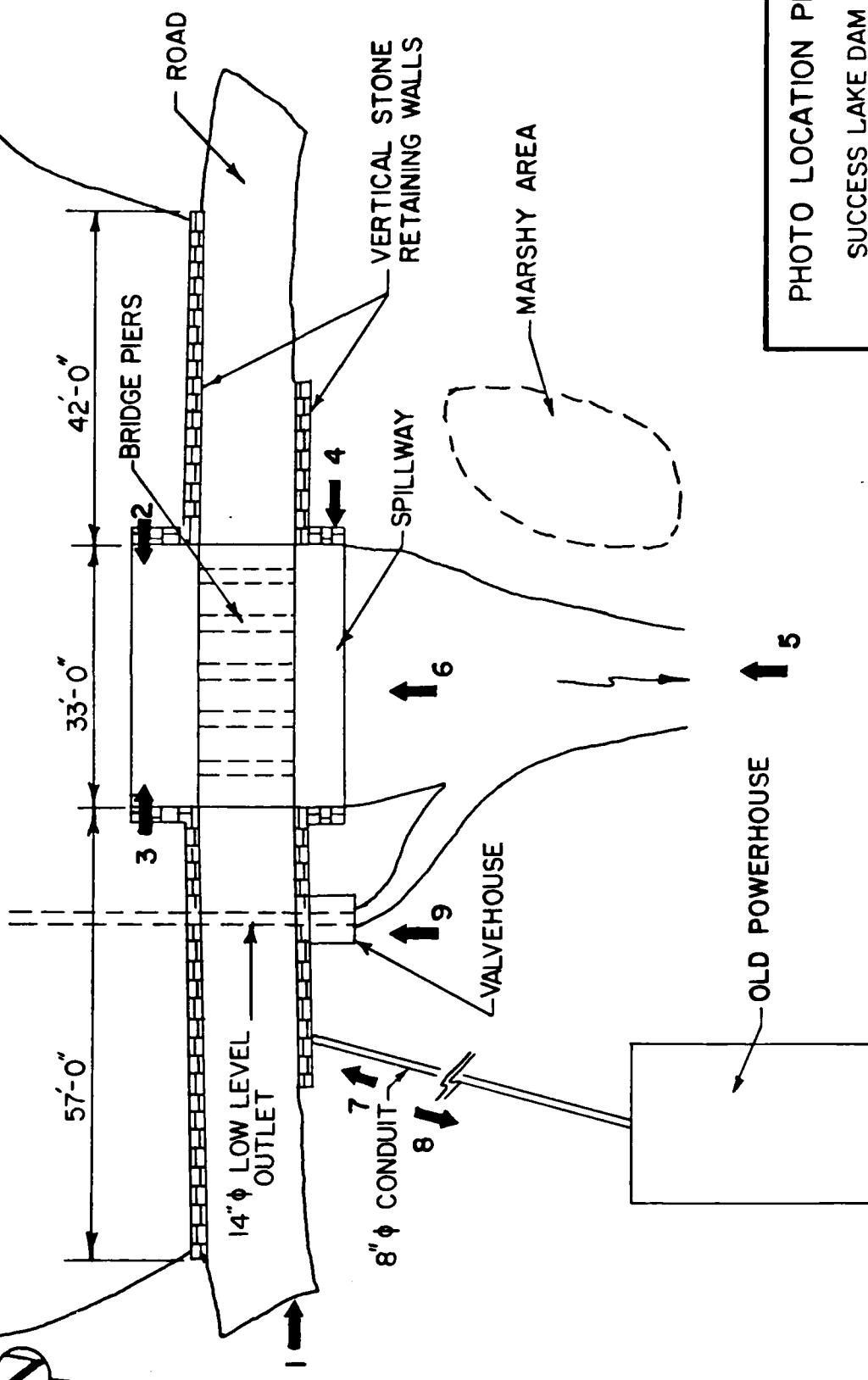


PHOTO LOCATION PLAN

SUCCESS LAKE DAM



Photo 1 Top of dam and single lane road.



Photo 2 Upstream face of dam, spillway crest and right  
dam embankment.

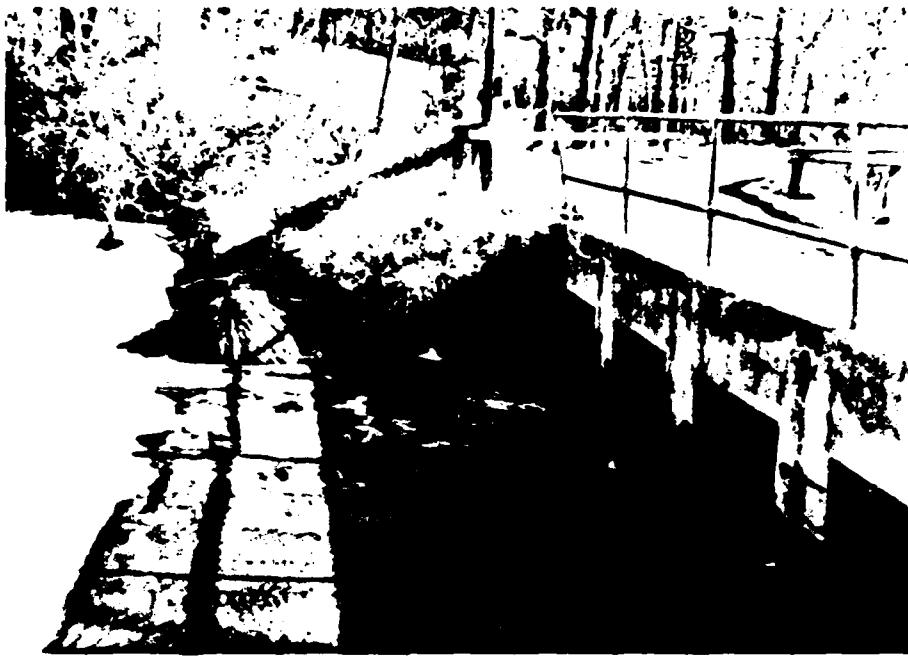


Photo 3 Upstream face of dam, spillway crest and left dam embankment.



Photo 4 Downstream spillway crest and bridge piers.



Photo 5 Downstream face of dam.



Photo 6 Downstream masonry face of spillway.



Photo 7 Downstream masonry face  
of right dam embankment,  
8 inch diameter conduit  
and control valve.



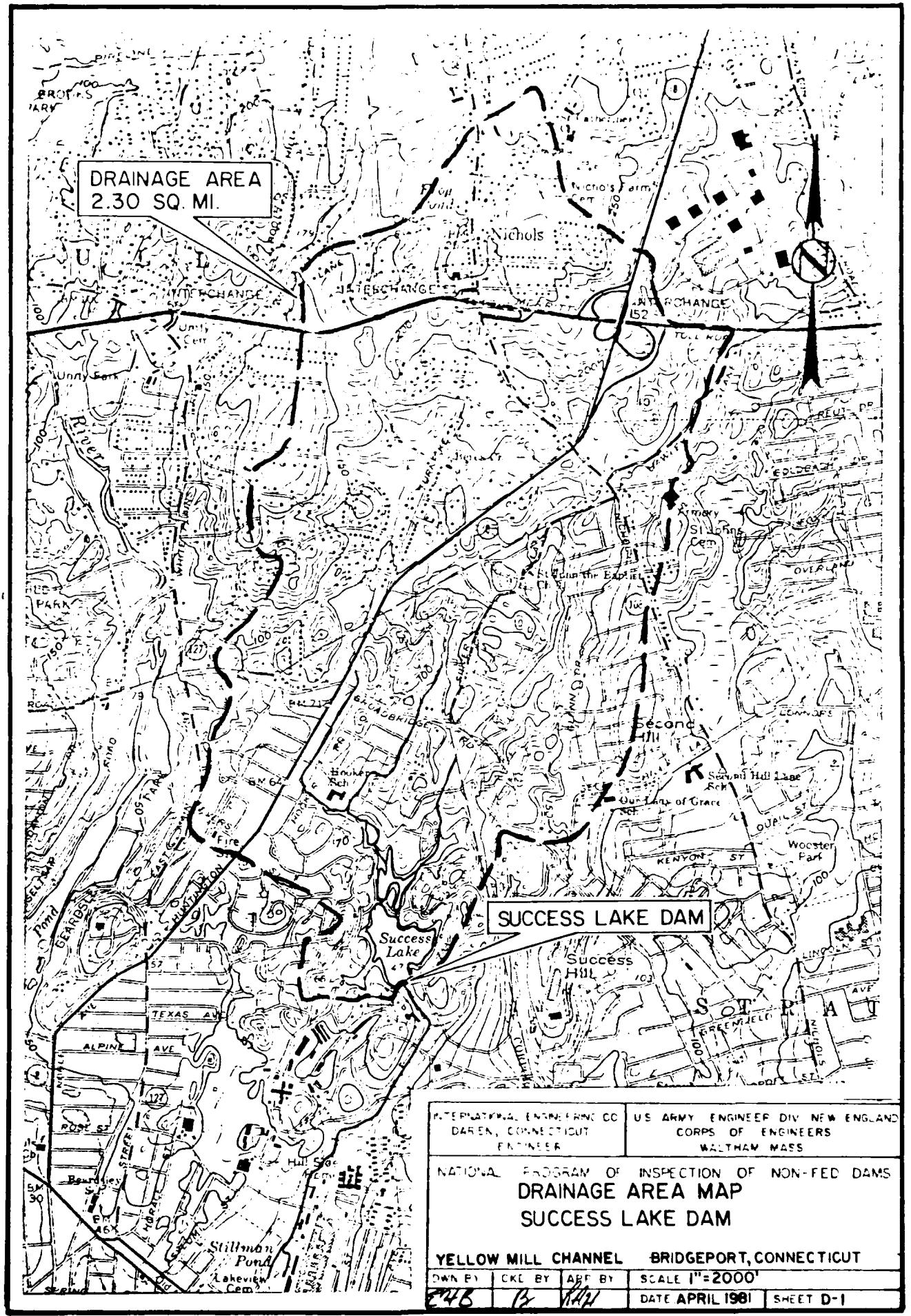
Photo 8 Brick structure and 8 inch diameter conduit.



Photo 9 Low-level outlet and valvehouse.

**APPENDIX D**

**HYDROLOGIC AND HYDRAULIC COMPUTATIONS**





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Project NATIONAL DAM INSPECTION PROGRAM (NDIP) Contract No. Z616-04  
Feature SUCCESS LAKE DAM, BRIDGEPORT, CT Designed MJF  
Item CT00079 Checked AJF

Sheet D-1

File No.

Date 3/10/81

Date

## HYDRAULIC / HYDROLOGIC INSPECTION

SUCCESS LAKE DAM, BRIDGEPORT, CT CT00079

I. PERFORMANCE AT PEAK FLOOD CONDITIONS

## 1. MAXIMUM PROBABLE FLOOD

a. WATERSHED CLASSIFIED AS "ROLLING"

b. WATERSHED AREA (D.A.) = 2.30 SQ. MI. \*

\* FROM IECO MEASUREMENTS ON THE BRIDGEPORT USGS QUADRANGLE MAP, CT. FROM U.S. CORPS OF ENGINEERS (ACE) DATA, D.A. IS 2.13 SQ. MI.

c. EXTRAPOLATING FROM NED-ACE GUIDE CURVES

$$\text{PMF} \approx 2080 \text{ cfs / sq. mi.}$$

d. THEREFORE, PEAK INFLOW:

$$\text{PMF} = 2080 \times 2.3 \approx 4780 \text{ cfs}$$

$$\frac{1}{2} \text{ PMF} \approx 2390 \text{ cfs}$$

2. SURCHARGE AT PEAK INFLOWS (PMF AND  $\frac{1}{2}$  PMF).

## a. OUTFLOW RATING CURVE

## i. SPILLWAY

THE MASONRY SPILLWAY IN THE MID-SECTION OF SUCCESS LAKE DAM IS

A BROAD-CRESTED WEIR WITH A VERTICAL DOWNSTREAM FACE

(SEE SKETCHES ON P.D-2).



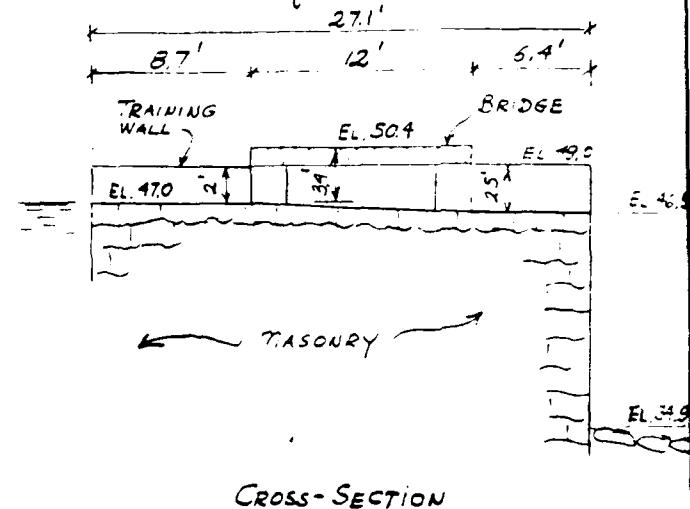
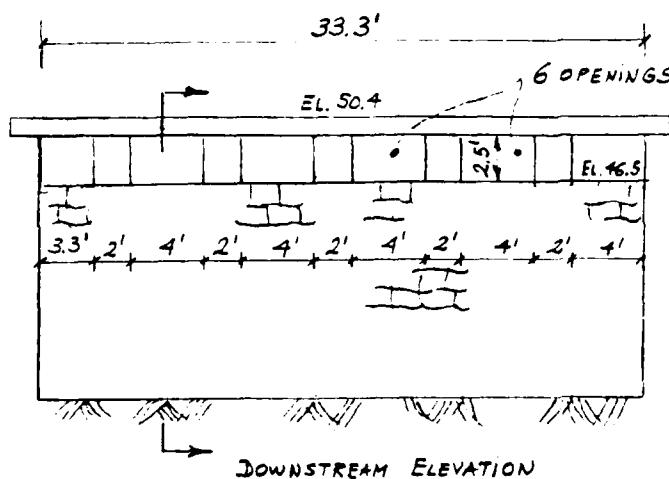
D-1



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Project NOJO  
 Feature SUCCESS LAKE DAM  
 Item \_\_\_\_\_

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 Contract No. 266-C  
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THE 33.3-FT-WIDE AND 27.1-FT-LONG SPILLWAY HAS A CONCRETE ROAD BRIDGE

WITH 6 OPENINGS THE FIVE OF WHICH HAVE A WIDTH OF 4 FT AND THE ONE  
 OPENING ON THE RIGHT SIDE IS A 3.3-FT WIDE. THE HEIGHT OF THE OPENINGS IS  
 2 FT ON THE UPSTREAM BRIDGE EDGE AND 2.5 FT ON THE DOWNSTREAM EDGE.

THE TOTAL LENGTH OF THE OPENINGS IS 23.3 FT ( $L_o$ ) AND THE TOTAL AREA OF

THE OPENINGS ON THE UPSTREAM SIDE IS 46.6 SQ. FT ( $A_o$ ).

ASSUMING  $C_1 = 2.2$  ( $H < 2$  FT) AND  $C_2 = 0.6$  ( $H > 2$  FT) AND ADOPTING

THE SPILLWAY CREST ELEV. 47.0 AS DATUM, THE SPILLWAY DISCHARGE IS

APPROXIMATING BY :

$$Q_s = C_1 L_o H_1^{3/2} + C_2 A_o \sqrt{2g(H_2 - \frac{3}{2})^{\frac{1}{2}}} = 2.2 \times 23.3 \times H_1^{3/2} + 0.6 \times 46.6 \times \sqrt{64.4(H_2 - \frac{3}{2})^{\frac{1}{2}}}$$

$$Q_s = 51.3 H_1^{3/2} + 224.4(H_2 - \frac{3}{2})^{\frac{1}{2}} \quad (\text{WHEN } H_1 < 2 \text{ FT}, H_2 = \frac{3}{2}; \text{ WHEN } H_2 > 2, H_1 = 0)$$





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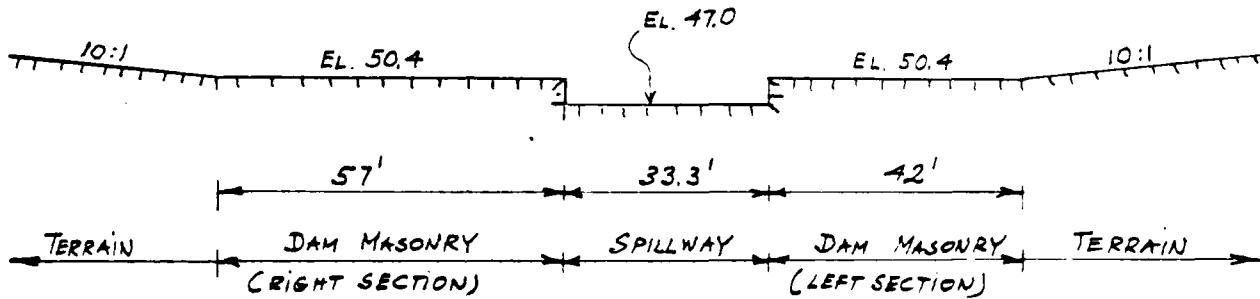
Sheet D-3

Project NDIP  
 Feature SUCCESS LAKE DAM  
 Item

Contract No. E616-54 File No.  
 Designed MP Date 3/10/54  
 Checked JF Date

ii. EXTENTION OF THE RATING CURVE FOR SURCHARGE OVERTOPPING THE DAM AND/OR ADJACENT TERRAIN

THE SUCCESS LAKE DAM IS A MASONRY STRUCTURE WITH A TOP ELEVATION OF 50.4 AND TOTAL LENGTH OF 99 FT. THE TERRAINS ADJACENT TO THE DAM HAVE SLOPES APPROXIMATELY 10:1 (SEE SKETCH BELOW).



DUE TO THE IRREGULARITIES IN THE PROFILE AN EQUIVALENT WEIR LENGTH MUST BE COMPUTED. ASSUMING A DISCHARGE COEFFICIENT  $C=2.3$  AND ADOPTING THE SPILLWAY CREST AS DATUM (EL. 47.0), THE OVERFLOW CAN BE APPROXIMATED BY THE FOLLOWING EQUATIONS:

(1) TOP OF DAM AT EL. 50.4.

$$Q_d = 2.3 \times \frac{132.3}{125.3} \times (H_3 - 3.4)^{3/2} = 304.3 (H_3 - 3.4)^{3/2}, \quad (H_3 > 3.4 \text{ ft})$$

(2) SLOPING TERRAIN TO THE LEFT AND RIGHT OF THE DAM:

$$L_s = \left(\frac{2}{5}\right) Z (H_3 - 3.4) = \left(\frac{2}{5}\right) 10 (H_3 - 3.4) = 4(H_3 - 3.4)$$

$\therefore$  DISCHARGE OVER LEFT AND RIGHT TERRAINS

$$Q_s = 2L_s (H_3 - 3.4)^{3/2} = 2 \times 4 (H_3 - 3.4)^{5/2} = 8 (H_3 - 3.4)^{5/2}$$





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SUCCESS LAKE DAM

Item

Contract No. 2616-C4

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File No.

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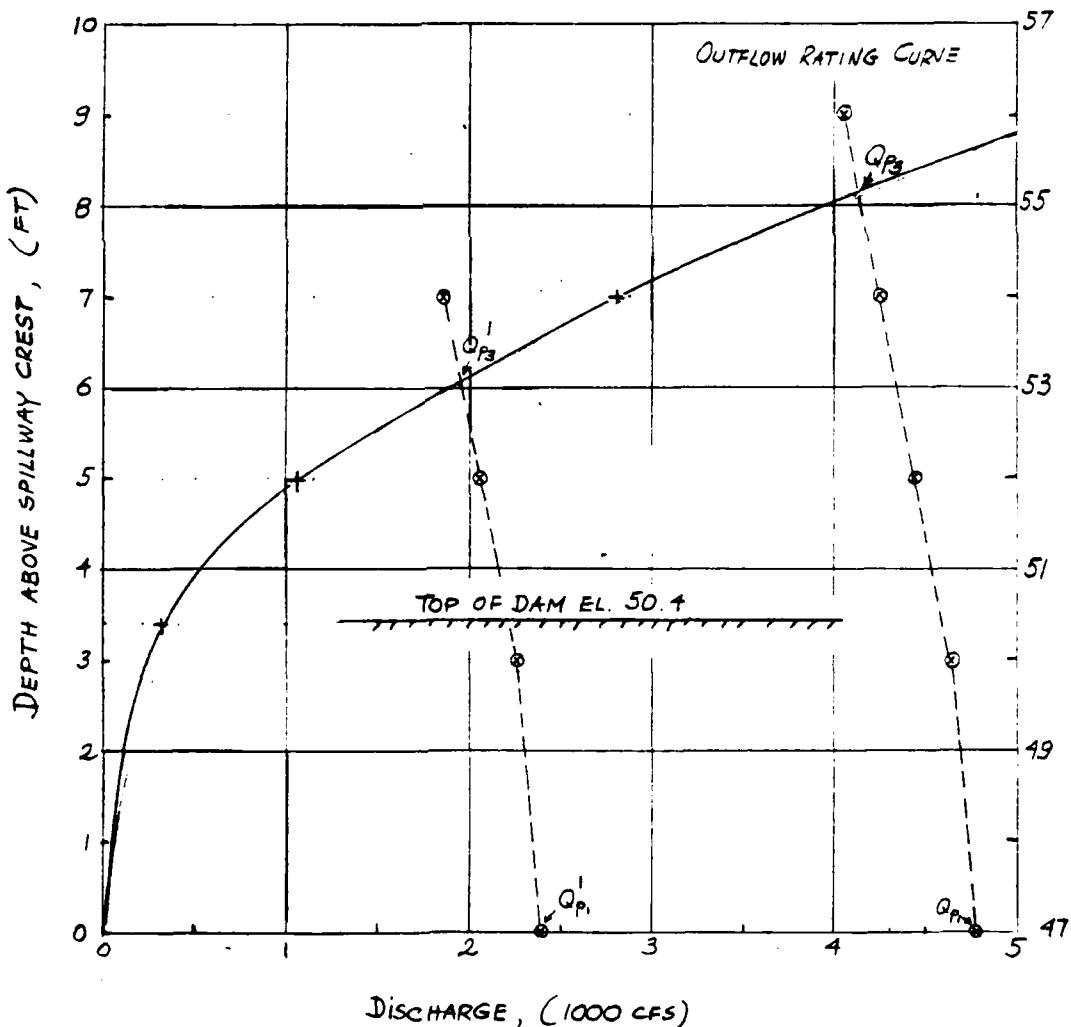
Date

THEREFORE, THE TOTAL OUTFLOW RATING CURVE IS APPROXIMATED BY:

$$Q = 51.3 H_1^{3/2} + 224.4 \left(H_2 - \frac{3}{2}\right)^{\frac{1}{2}} + 304.3 \left(H_3 - 3.4\right)^{3/2} + 8 \left(H_3 - 3.4\right)^{5/2} \quad H_3 \geq 3.4$$

WHEN  $H_1 < 2$  FT,  $H_2 = \frac{3}{2}$ ; WHEN  $H_2 > 2$ ,  $H_1 = 0$ 

THE RESULTING OUTFLOW RATING CURVE IS AS FOLLOWS:



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Sheet D-5

Feature

SUCCESS LAKE DAM

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Date

b. SURCHARGE HEIGHT TO PASS PEAK INFLOWS ( $Q_p$  AND  $Q_p'$ )

i. @  $Q_p = 4780 \text{ CFS}$   $H_s \approx 8.6 \text{ FT}$

ii. @  $Q_p' = 2390 \text{ CFS}$   $H_s' \approx 6.6 \text{ FT}$

## c. EFFECT OF SURCHARGE STORAGE ON PEAK OUTFLOWS :

## i. AVERAGE POND AREA WITHIN EXPECTED SURCHARGE:

(1) POND AREA AT FLOW LINE (EL. 47.0)  $A_{47}^* = 12.85 \text{ AC}$

(2) POND AREA AT EL. 50.0  $A_{50}^* = 30.3 \text{ AC}$

(3) AREA AT CONTOUR 60.0  $A_{60}^* = 68.8 \text{ AC}$

\* FROM IECO MEASUREMENTS ON THE BRIDGEPORT USGS QUADRANGLE MAP, CT

ASSUMING NORMAL POOL AT SPILLWAY CREST EL. 47.0, APPROXIMATING

STAGE-STORAGE RATING CURVE WAS CONSTRUCTED (SEE A D-6).

ii. DISCHARGE ( $Q_p$ ) AT VARIOUS HYPOTHETICAL SURCHARGE ELEVATIONS:

$H = 9 \text{ FT}, \quad V = 362 \text{ AC-FT}, \quad \therefore S = \frac{362}{2.3 \times 53.3} = 2.95 \text{ IN}$

$H = 7 \text{ FT}; \quad V = 262 \text{ AC-FT}; \quad S = 2.14 \text{ IN}$

$H = 5 \text{ FT}; \quad V = 162 \text{ AC-FT}; \quad S = 1.32 \text{ IN}$

$H = 3 \text{ FT}; \quad V = 65 \text{ AC-FT}; \quad S = 0.53 \text{ IN}$



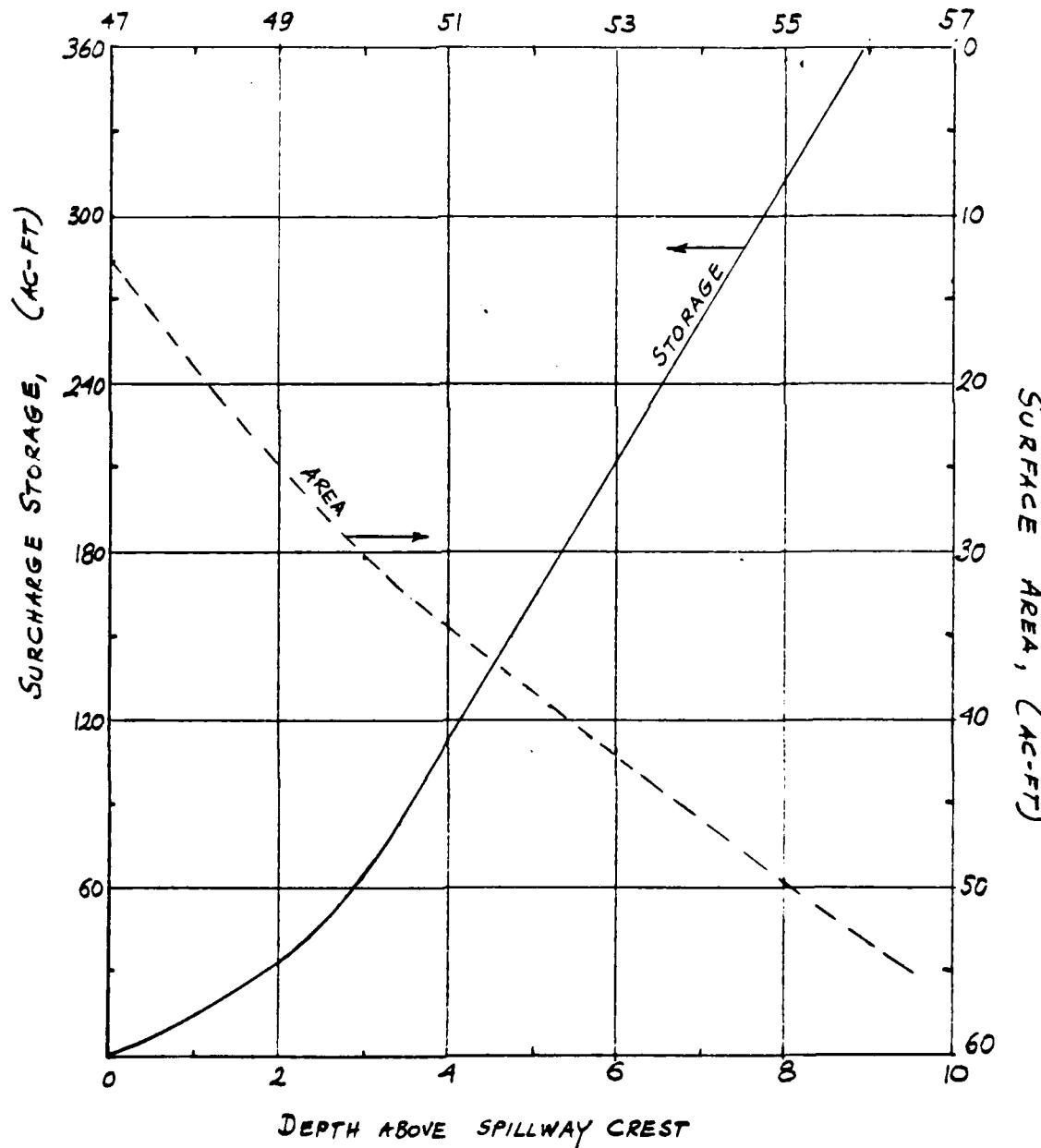


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Feature SUCCESS LAKE DAM  
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Date \_\_\_\_\_

## STAGE-STORAGE AND STAGE-AREA CURVES

SURFACE ELEVATIONS, (FT- NGVD)





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Project NDIP      Contract No. AE 5-C2      Sheet D-7  
 Feature SUCCESS LAKE DAM      Designed M.P      File No.   
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FROM APPROXIMATE ROUTING NED-ACE GUIDELINES AND 19' N. MAXIMUM PROCEPARE

RUNOFF IN NEW ENGLAND:

$$Q_{P_2} = Q_P \left(1 - \frac{s}{19}\right) \text{ AND FOR } \frac{1}{2} \text{ PMF. } Q_{P_2}' = Q_P' \left(1 - \frac{s}{9.5}\right)$$

∴ FOR THE PREVIOUS HYPOTHETICAL SURCHARGES:

$$H = 9 \text{ FT; } Q_{P_2} = 4038 \text{ cfs; } Q_{P_2}' = 1648 \text{ cfs}$$

$$H = 7 \text{ FT; } Q_{P_2} = 9242 \text{ cfs; } Q_{P_2}' = 1852 \text{ cfs}$$

$$H = 5 \text{ FT; } Q_{P_2} = 4418 \text{ cfs; } Q_{P_2}' = 2058 \text{ cfs}$$

$$H = 3 \text{ FT; } Q_{P_2} = 9647 \text{ cfs; } Q_{P_2}' = 2257 \text{ cfs}$$

d. PEAK OUTFLOWS ( $Q_{P_3}$  AND  $Q_{P_3}'$ ):

USING NED-ACE GUIDELINES "SURCHARGE STORAGE ROUTING" ALTERNATE

METHOD AND RATING CURVE (SEE P. D-4):

$$Q_{P_3} = 4120 \text{ cfs} \quad H_3 = 8.1 \text{ FT}$$

$$Q_{P_3}' = 1950 \text{ cfs} \quad H_3' = 6.05 \text{ FT}$$

3. SPILLWAY CAPACITY RATIO TO PEAK INFLOW AND OUTFLOW.

SPILLWAY CAPACITY TO TOP OF DAM (EL. 50.4) IS 309 cfs

% CAPACITY OF INFLOW PMF : 6

" OUTFLOW " : 8

" INFLOW 1/2 PMF : 13

" OUTFLOW " : 16



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SUCCESS LAKE DAM

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## II. DOWNTSTREAM FAILURE HAZARD

### 1. POTENTIAL IMPACT AREA

THE POTENTIAL IMPACT AREA IS LOCATED 3500 FT DOWNSTREAM FROM THE DAM

LARGE 5-STORY CONCRETE BUILDING

NEAR BOND STREET, HAS FIRST FLOOR ELEVATION ABOUT 20 FT ABOVE

THE STREAMBED. THERE IS ALSO THE STATE ROUTE 1 BRIDGE LOCATED

ABOUT 1/3 MILES DOWNSTREAM FROM THE DAM.

### 2. FAILURE OF SUCCESS LAKE DAM.

#### a. BREACH WIDTH

##### i. HEIGHT OF DAM:

TOP OF DAM EL. 50.4 ; DAM DOWNSTREAM TOE 34.9;  $\therefore H = 15.5 \text{ FT}$

ii. DAM MID-HEIGHT EL. 42.7  $(50.4 - 15.5/2 \approx 42.7)$

iii. APPROXIMATE MID-HEIGHT LENGTH:  $\ell^* \approx 50 \text{ FT}$  (SPILLWAY LENGTH IS NOT INCLUDED)

\* FROM IECO DRAWINGS

#### iv. BREACH WIDTH (SEE NED-ACE DOWNSTREAM FAILURE GUIDELINES)

$$N_b = 0.4 \quad C = 0.4 \times 50 = 20 \text{ FT}$$

#### b. PEAK FAILURE OUTFLOW ( $Q_{p_f}$ )

ASSUME SURCHARGE AT TOP OF DAM (EL. 50.4)





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SUCCESS LAKE DAM

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Contract No. 2616-C4

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i. HEIGHT AT TIME OF FAILURE :  $Y_0 = 15.5 \text{ FT}$ ii. SPILLWAY DISCHARGE AT TIME OF FAILURE :  $Q_s = 309 \text{ CFS}$ 

iii. BREACH OUTFLOW :

$$Q_b = \frac{8}{27} w_b \sqrt{g} Y_0^{3/2} = \frac{8}{27} \times 20 \times \sqrt{32.2} \times 15.5^{3/2} = 2052 \text{ CFS}$$

iv. PEAK FAILURE OUTFLOW TO YELLOW MILL CHANNEL TRIBUTARY

$$Q_p = Q_s + Q_b = 309 + 2052 = 2360 \text{ CFS}$$

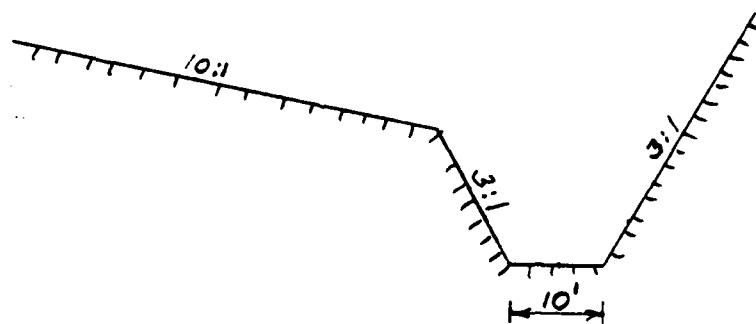
c. FLOOD DEPTH IMMEDIATELY DOWNSTREAM FROM DAM:

$$Y = 0.44 Y_0 = 0.44 \times 15.5 = 6.8 \text{ FT}$$

d. ESTIMATE OF DOWNSTREAM FAILURE CONDITIONS AT POTENTIAL IMPACT AREA  
(SEE NED-ACE GUIDELINES FOR ESTIMATING DOWNSTREAM FAILURE HYDROGRAPHS)

i. REACH OF YELLOW MILL CHANNEL TRIBUTARY BETWEEN DAM AND IMPACT AREA.

VARIABLES SIGNIFICANTLY IN SECTION. THE FIRST 1500-FOOT-LONG REACH IS APPROXIMATELY SHAPED AS SHOWN ON THE SKETCH BELOW:



CROSS SECTION REACH 1  
THE AVERAGE SLOPE OF THE REACH IS 0.002 (+)



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Feature SUCCESS LAKE DAM File No. \_\_\_\_\_  
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## ii SUCCESS LAKE DAM RESERVOIR STORAGE AT TIME OF FAILURE.

STORAGE VOLUME BELOW SPILLWAY CREST APPROXIMATED BY  $\frac{1}{4} \pi H^2$ 

$$= \frac{1}{4} \times 12.85 \times 12.1 = 38.9 \text{ AC-FT. SURCHARGE STORAGE TO THE TOP OF THE DAM}$$

(EL. 50.4) is 80.3 AC-FT (SEE STAGE - SURCHARGE CURVE ON P. D-6).

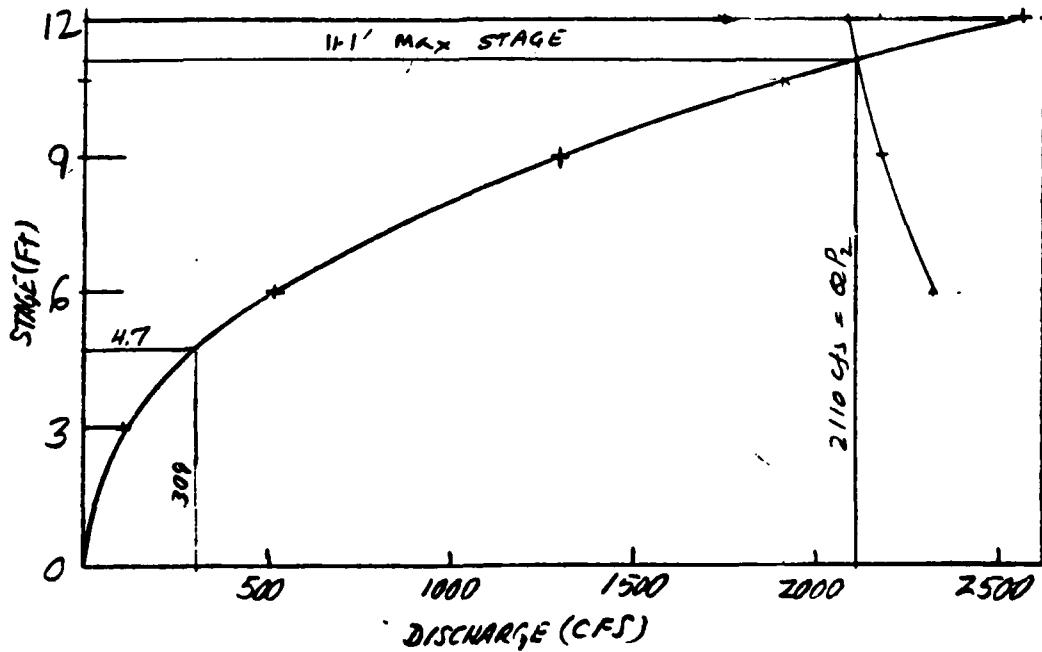
∴ MAXIMUM STORAGE VOLUME OF THE RESERVOIR IS  $38.9 + 80.3 = 119.2 \text{ AC-FT}$ ASSUME  $S_{MAX} = 119 \text{ AC-FT}$ iii PEAK INFLOW TO REACH:  $Q_{P_1} = 2360 \text{ CFS}$ 

## iv. APPROXIMATE STAGE AT POTENTIAL IMPACT AREA FAILURE OF SUCCESS LAKE DAM

REACH L = 3500 FT; n = 0.05; S = 0.002; COMPUTED STAGE - DISCHARGE

CURVE AND STAGE - AREA CURVE FOR THE BROOK SECTION AS SHOWN ON P.D-9

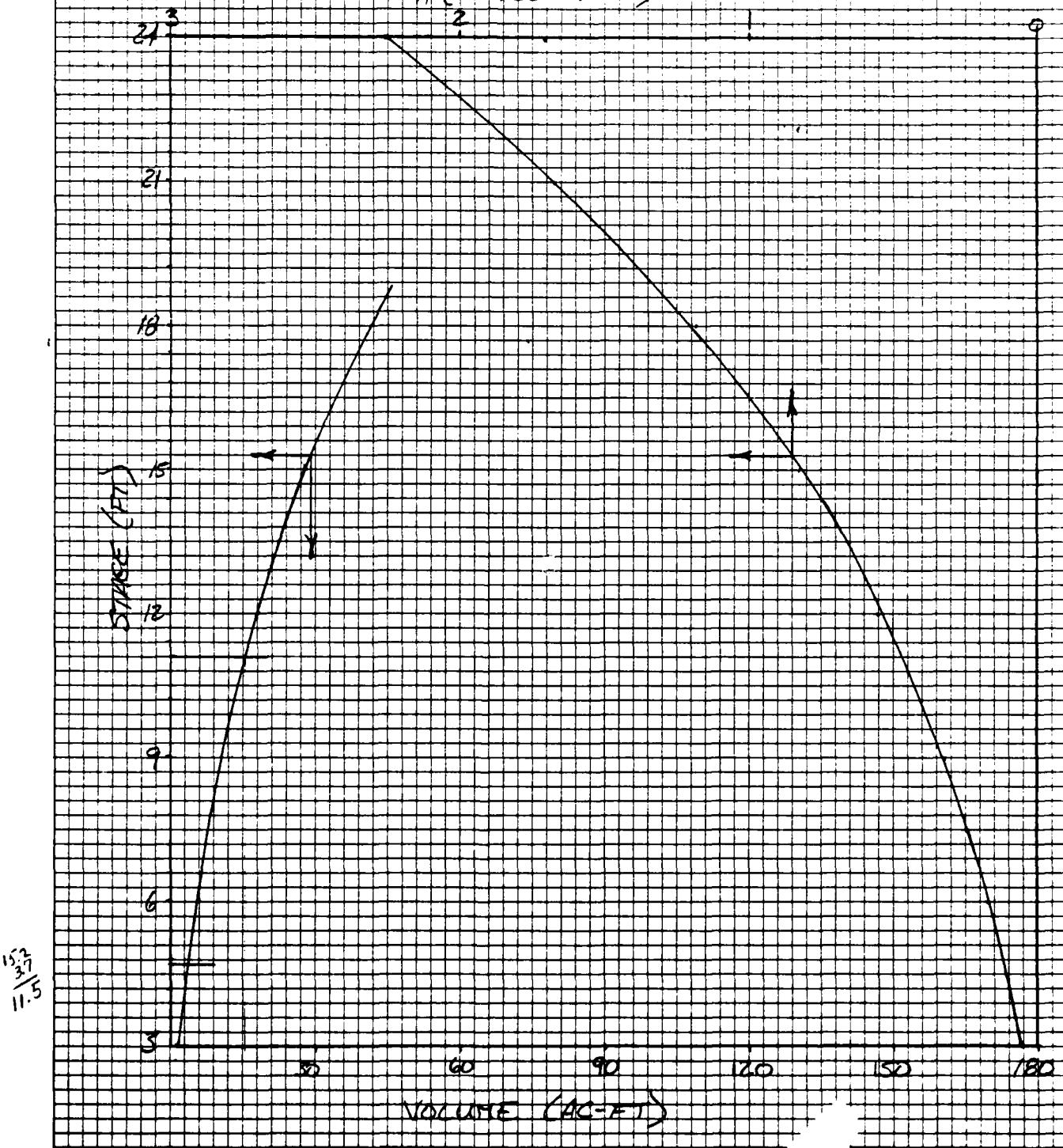
ARE PLOTTED ON P.D-11.

STAGE-DISCHARGE FOR CHANNEL - REACH 1

(-)

## AREA CAPACITY CURVE FOR FIRST REACH (1500 FEET LONG)

$A$  (in 1000 ft<sup>2</sup>)



**K-E** 10 X 10 TO THE INCH • 7 X 10 INCHES  
KEUFFEL & ESSER CO. MADE IN U.S.A.



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3/23/71

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PRE FAILURE STAGE 4.7FT DISCHARGE 309 CFS

INITIAL VOLUME ABSTRACTED &amp; AC-FT

H	V	$Q_{P2} = 2360 \left(1 - \frac{VOL-4}{119}\right)$
3	1.7	2406
6	6.0	2320
9	12.9	2183
12	18.1	2080

RISE IN STAGE 11.1 - 4.7 = 6.4'

$$Q_{P2} = 2110 \text{ CFS}$$





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 Feature SUCCESS LAKE DAM  
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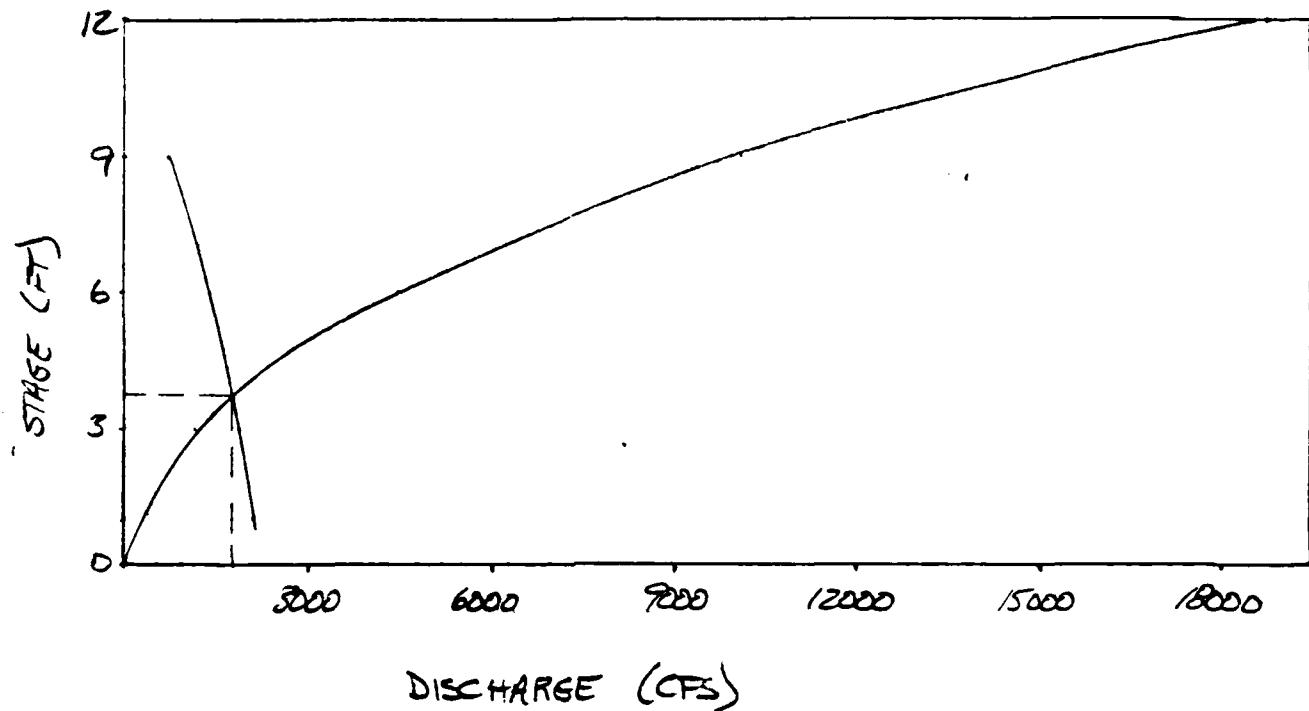
File No. \_\_\_\_\_

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Date \_\_\_\_\_

REACH 2:  $L = 1400\text{FT}$   $n = 0.05$   $s = 0.002$ 

STAGE DISCHARGE CURVE FOR REACH 2.



PRE FAILURE STAGE 1.0 FT DISCHARGE 309 CFS  
 INITIAL VOLUME ABSTRACTED  $V = 4.4 \text{ AC-FT}$   
 VOLUME ABSTRACTED BY REACH 1  $\Delta V_1 = 11.5 \text{ AC-FT}$   
 POTTING POINTS FOR GRAPHICAL ROUTINE

$$H \quad VOL \quad Q_{P2} = 2110 \left( 1 - \frac{VOL - 4.4}{119 - 115} \right)$$

$$1 \quad 4.4 \quad 2110$$

$$3 \quad 16.06 \quad 1881$$

$$6 \quad 41.07 \quad 1390$$

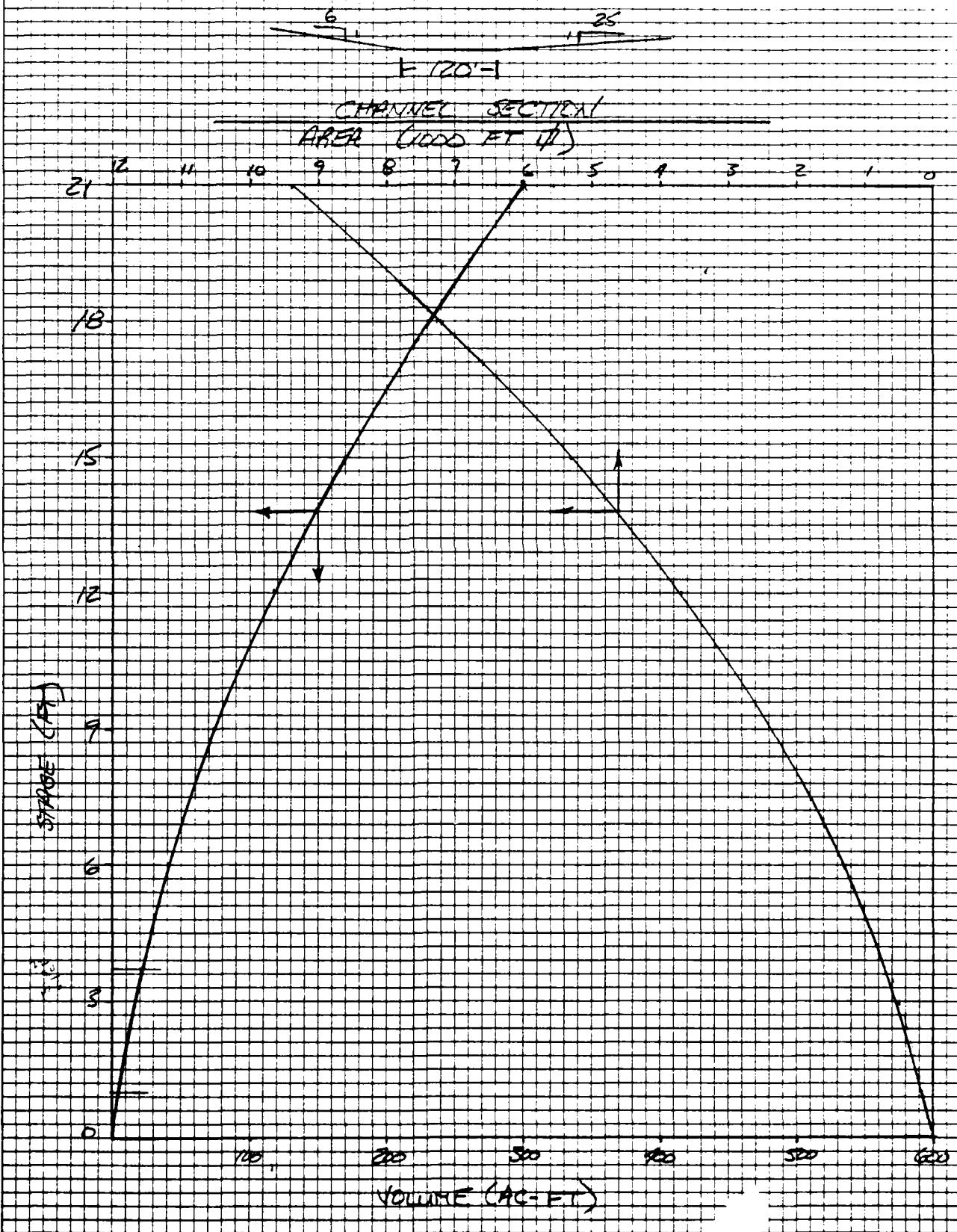
$$9 \quad 75.04 \quad 723$$

$$Q_{P2} = 1800 \text{ cfs} \quad H = 3.7 \text{ FT} \quad \Delta H = 2.7 \text{ FT}$$



D-14 B TF

AREA CAPACITY CURVE FOR SECONDS REACH  
(100 FEET LONG)





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Project NDPSheet D-15Feature SUCCESS LAKE DAMContract No. Z616

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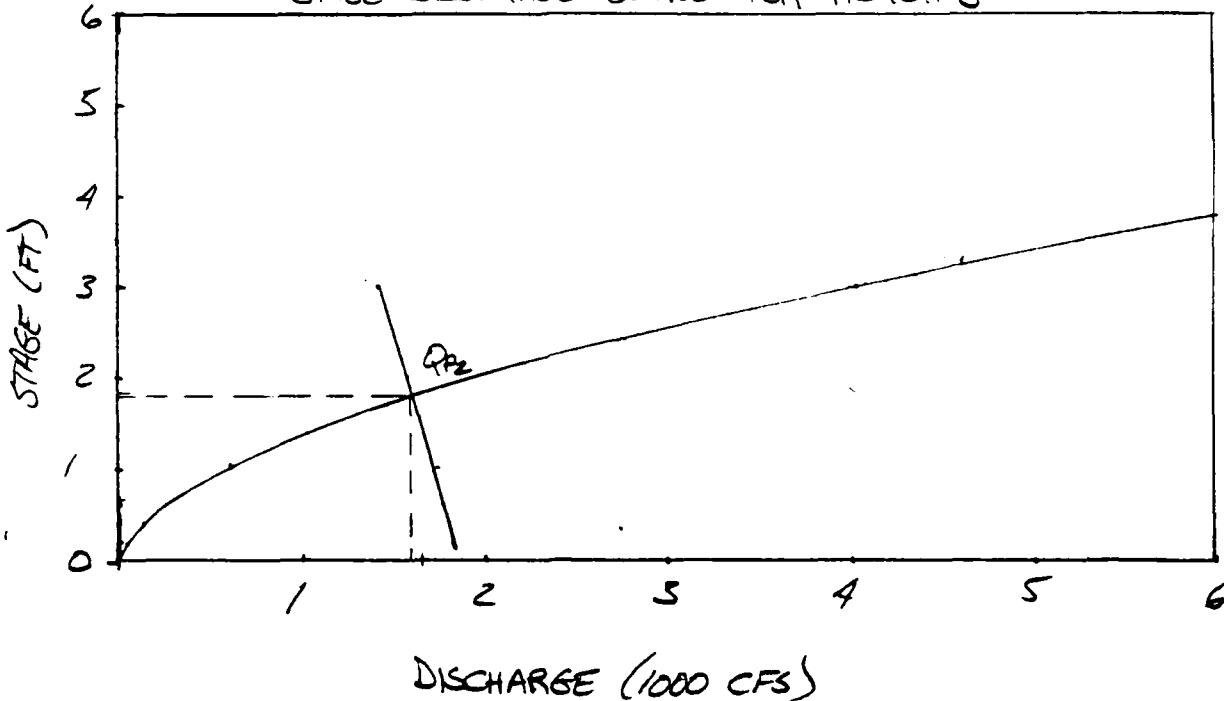
Item \_\_\_\_\_

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REACH 3: L = 600 FT N = 0.05 S = 0.002

STAGE DISCHARGE CURVE FOR REACH 3



PREFAILURE STAGE  $\approx 0.7$  FT DISCHARGE 309 CFS

INITIAL VOLUME ABSTRACTED  $\approx 3$  AC-FT

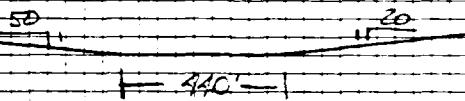
$$H \quad VOL \quad Q_{P_2} = 1800 \left(1 - \frac{VOL^3}{119-17.5}\right)$$

0.2	1.2	1836
0.6	3.8	1784
1.0	6.5	1730
1.4	9.1	1672
2.0	14.0	1580
3.0	22.5	1410



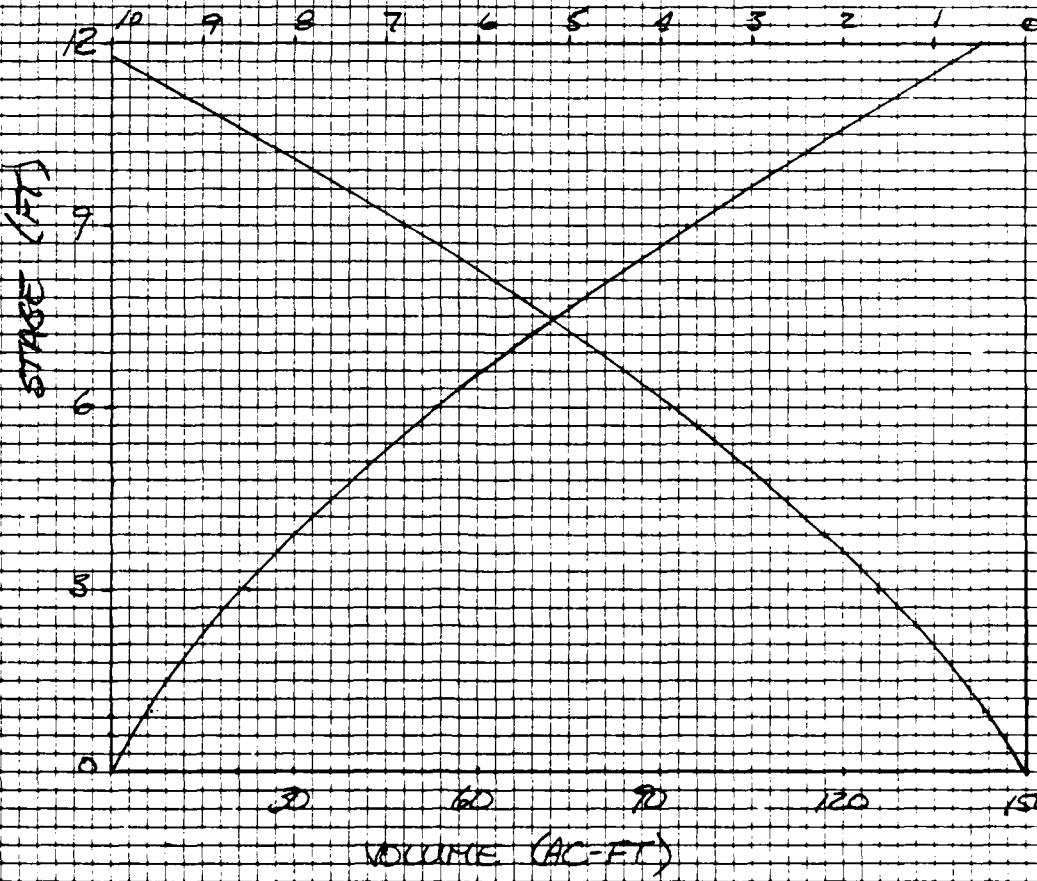
R-5E R-16

AREA CAPACITY CURVE FOR THIRD  
REACH ( $L = 600\text{FT}$ )



CHANNEL SECTION  
THIRD REACH

AREA (1000 FT L)





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$$Q_{P_2} = 1620 \text{ CFS} \quad H = 1.8 \text{ FT}$$

$$\text{RISE IN STAGE } \Delta H = 1.8 - 0.7 = 1.1 \text{ FT}$$

III. THE RISE IN STAGE WITHIN THE FIRST REACH  
WILL NOT EFFECT THE STRUCTURE IMMEDIATELY D/S  
FROM THE DAM (1ST FLOOR EL  $\approx$  20FT ABOVE STREAM BED)  
THE RISE IN STAGE WITHIN THE THIRD REACH WILL  
HAVE LITTLE OR NO EFFECT ON THE STRUCTURES NEAR  
THE STREAM.





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